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DEPARTMENT OF  
MECHANICAL ENGINEERING

# Sequential algorithms for the numerical analysis of delaminations: a new efficient and versatile approach

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# LUCA M. MARTULLI



**2010 - 2016**

**Bachelor/Master degree in Aerospace Engineering  
University of Pisa**



**2017 - 2020**

**PhD in Materials Engineering  
Toyota Motor Europe & KU Leuven**



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**2020 - Present**

**Assistant Professor  
Mechanical Engineering Department,  
Politecnico di Milano**





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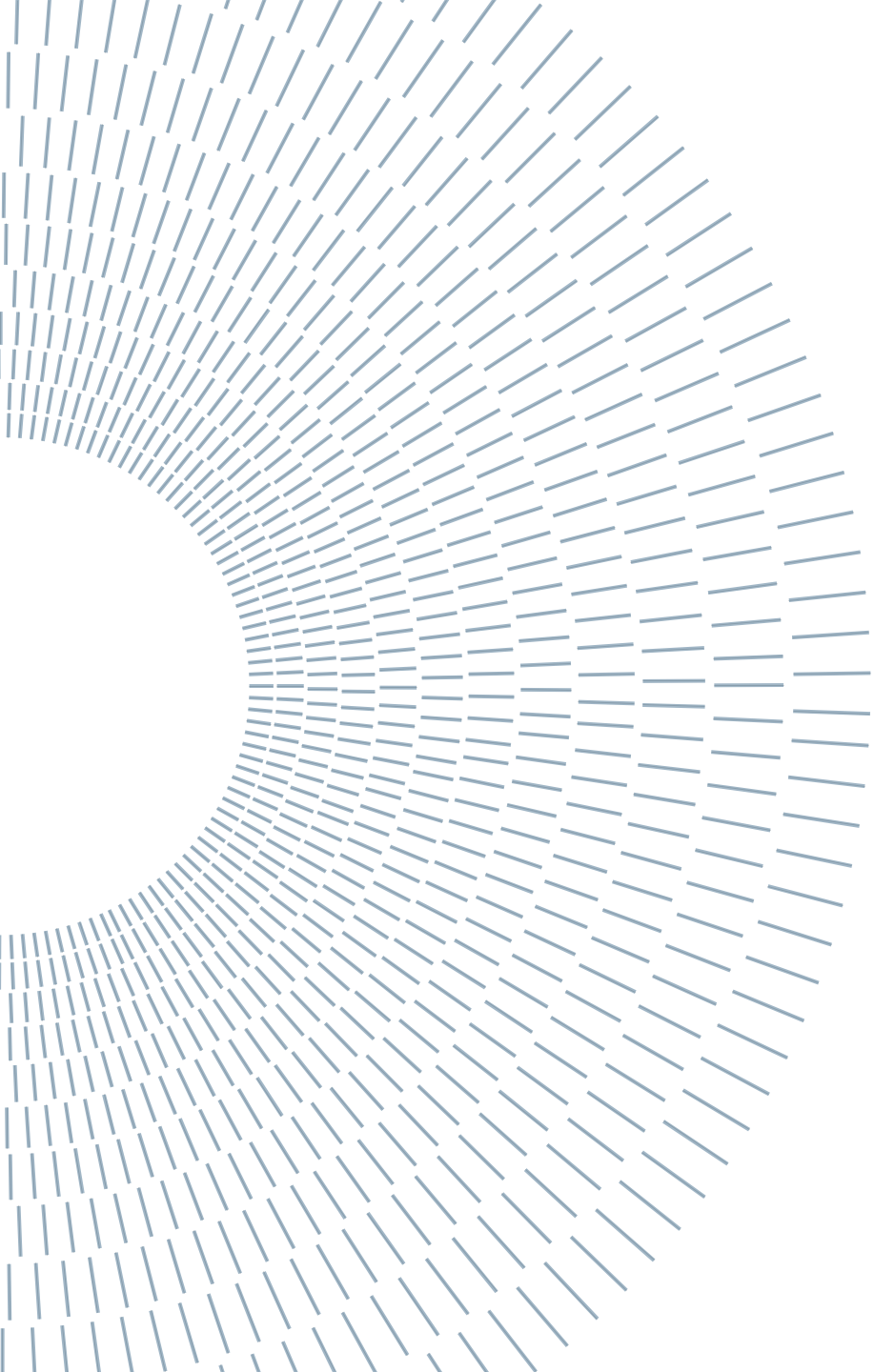
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# Sequential algorithms for the numerical analysis of delaminations: a new efficient and versatile approach

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# **SIMULATIONS OF DELAMINATIONS UNDER FATIGUE**

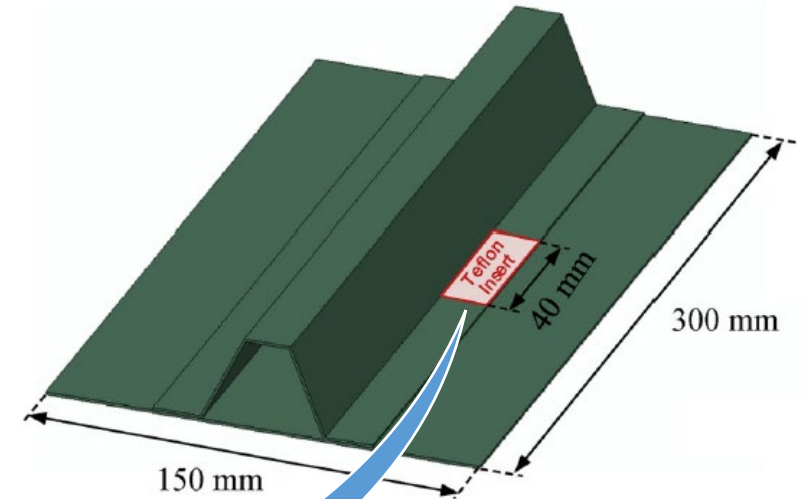
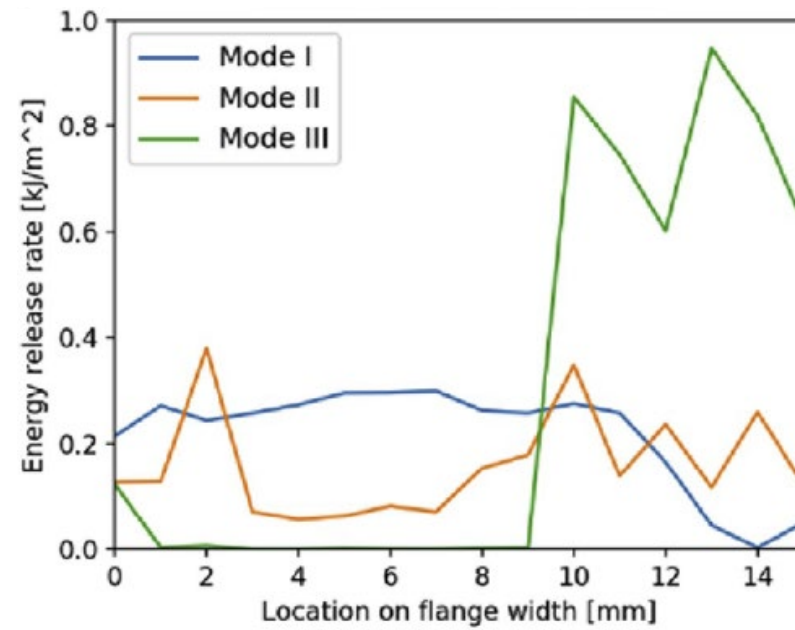


# THE BENCHMARK: THE DIRECT CYCLIC (DC) ALGORITHM

- Highly inefficient: from 2 to 15 more computationally expensive than cohesive zone models [1]
- Input limited to a single set of Paris parameters [1,2]

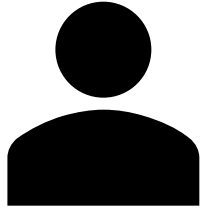
$$\frac{da}{dN} = C G^m$$

- [1] Pirondi et al. (2014)  
[2] Raimondo et al. (2020)

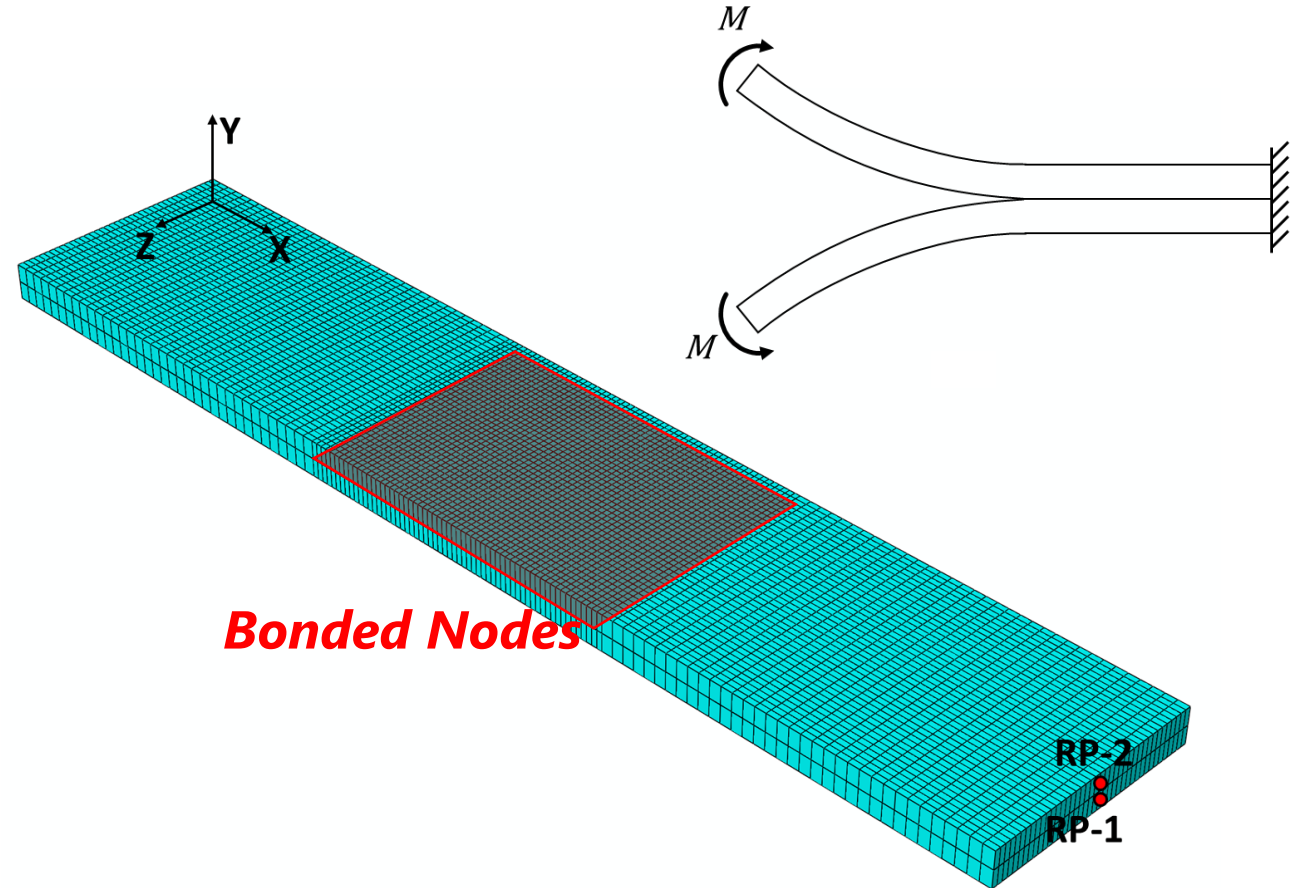




# OUR APPROACH: SEQUENTIAL-STATIC FATIGUE (SSF)



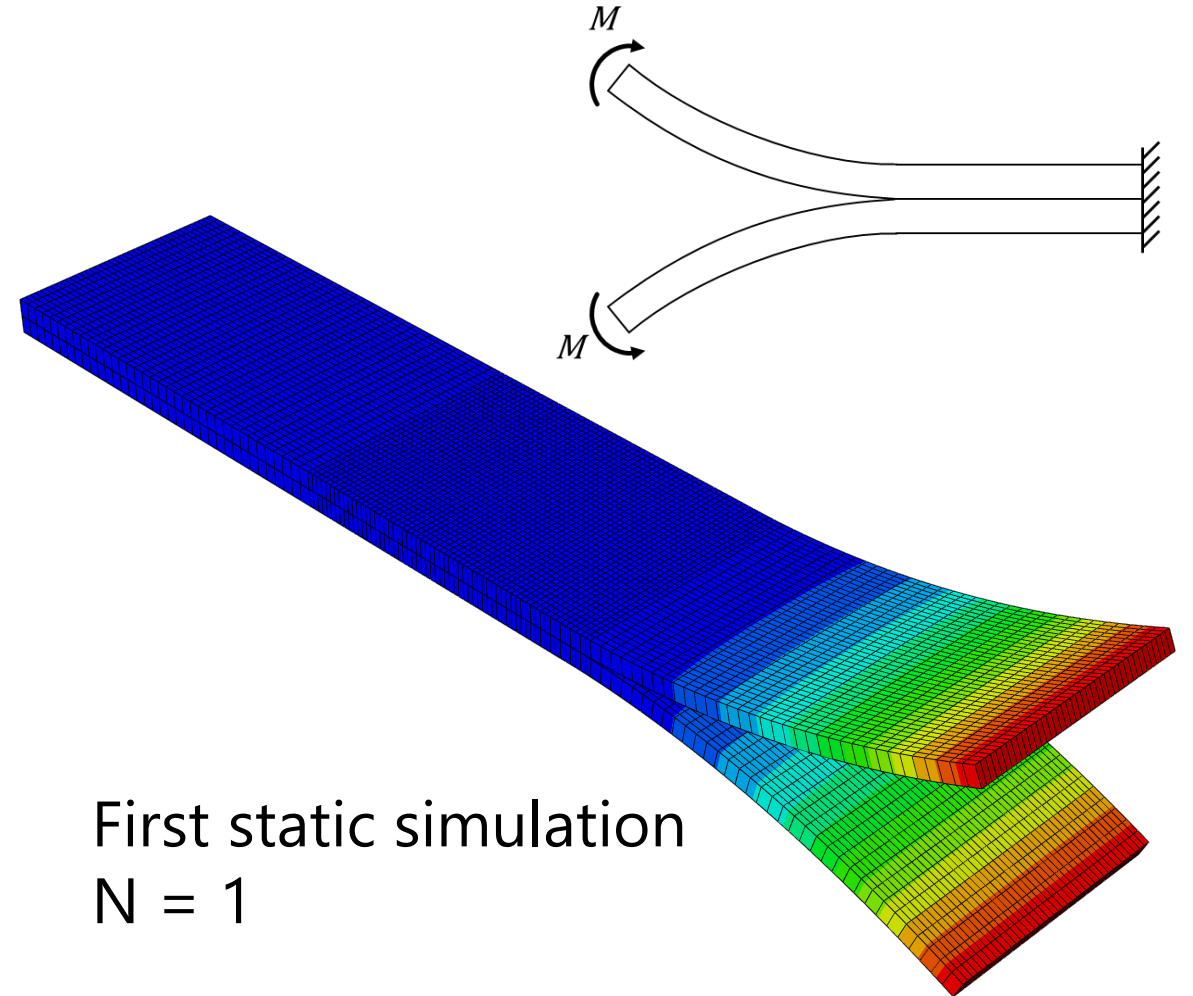
- Pre-processing



# OUR APPROACH: SEQUENTIAL-STATIC FATIGUE (SSF)



- Pre-processing
- **Launch simulation**



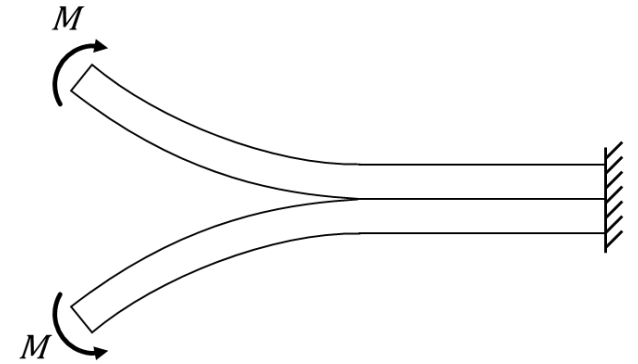
First static simulation  
 $N = 1$



# OUR APPROACH: SEQUENTIAL-STATIC FATIGUE (SSF)



- Pre-processing
- Launch simulation
- **SERR extraction**
- **Calculation of number of cycles to release one node**



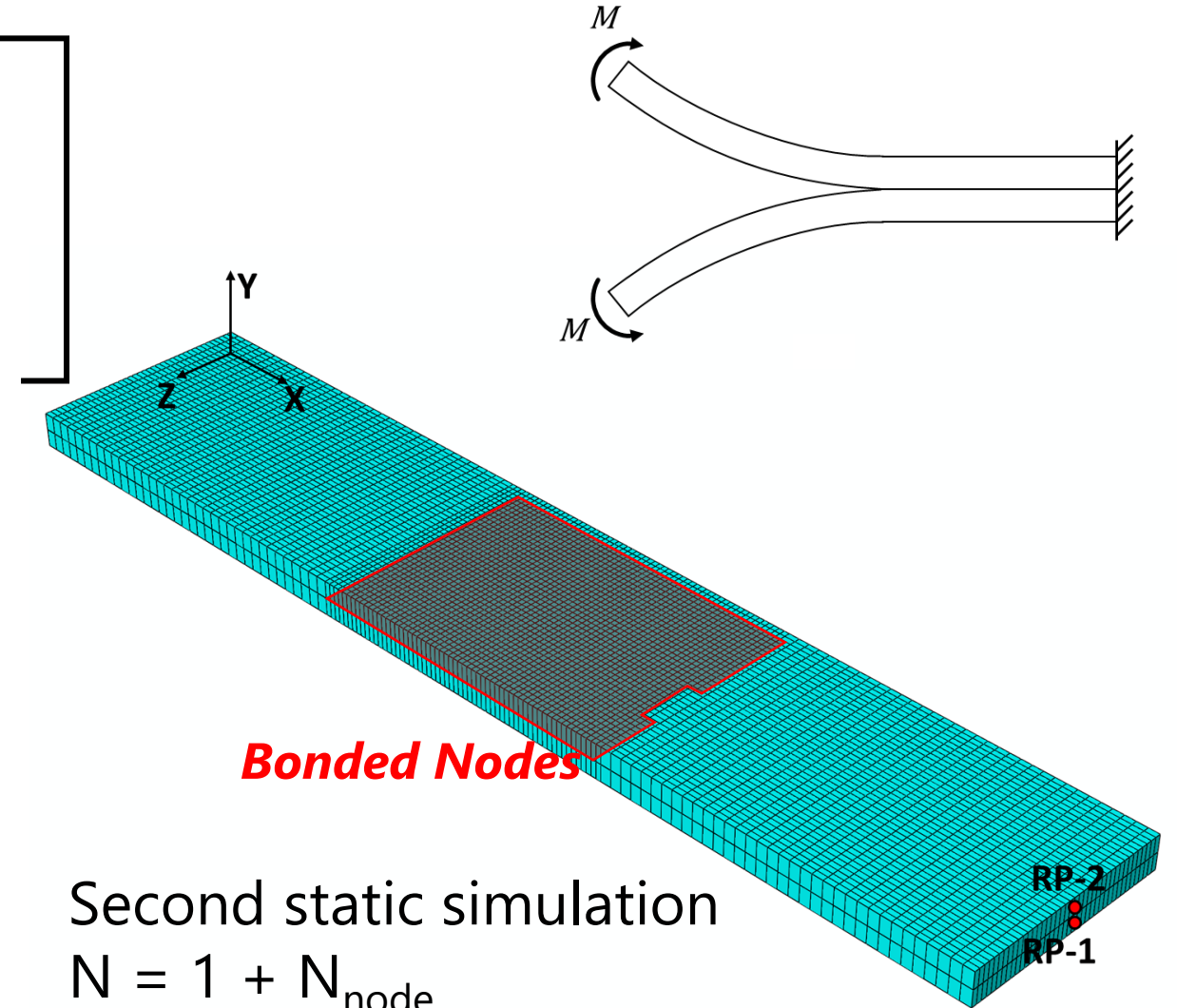
$$\frac{da}{dN} = f \left( \mathcal{G}_{\max}, \mathcal{G}_{\min}, \frac{\mathcal{G}_{II} + \mathcal{G}_{III}}{\mathcal{G}_{tot}} \right)$$

$$a = l_{el} \longrightarrow \downarrow N_{node}$$

# OUR APPROACH: SEQUENTIAL-STATIC FATIGUE (SSF)



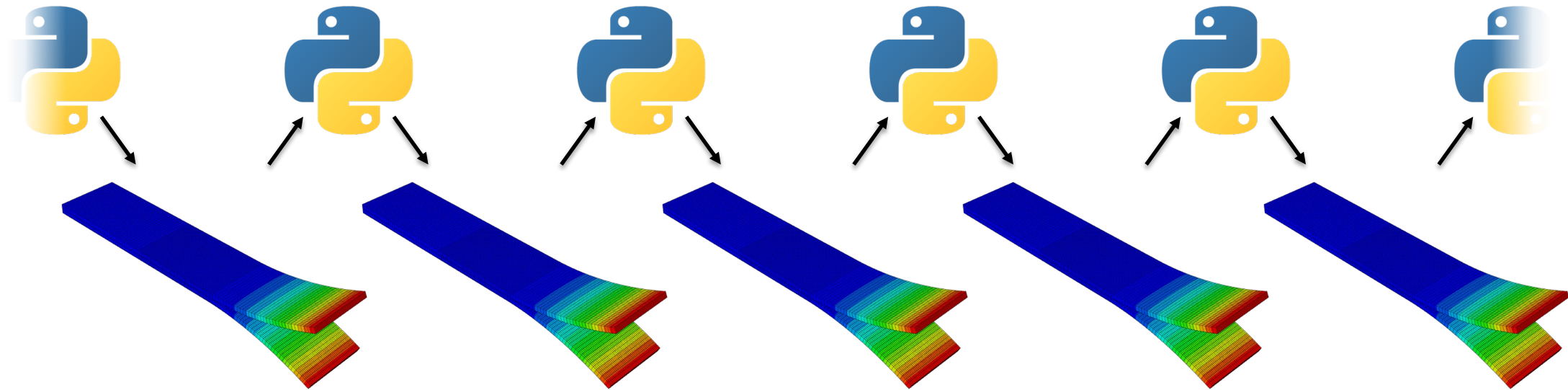
- Pre-processing
- Launch simulation
- SERR extraction
- Calculation of number of cycles to release one node



Second static simulation

$$N = 1 + N_{\text{node}}$$

# OUR APPROACH: SEQUENTIAL-STATIC FATIGUE (SSF)



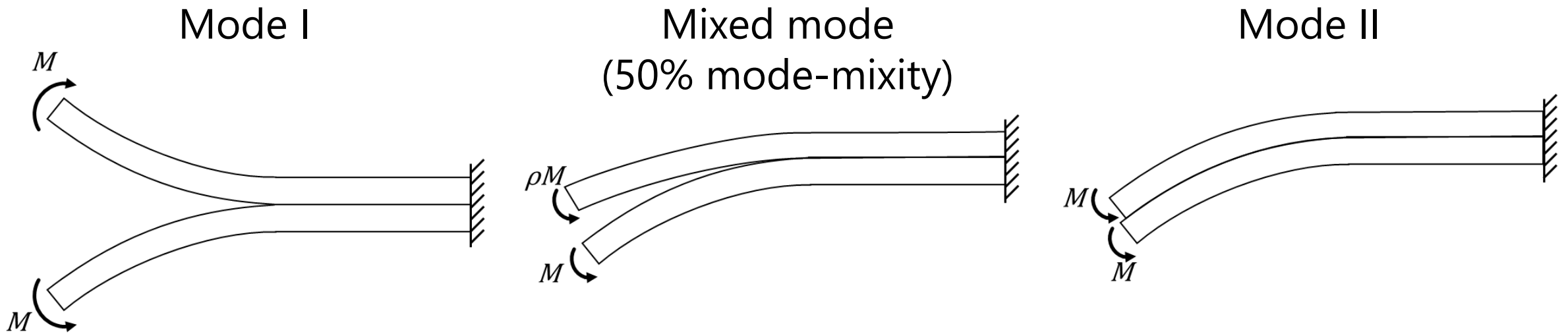
Fatigue load history is simulated via a series of static simulations

The algorithm uses the VCCT already implemented in Abaqus



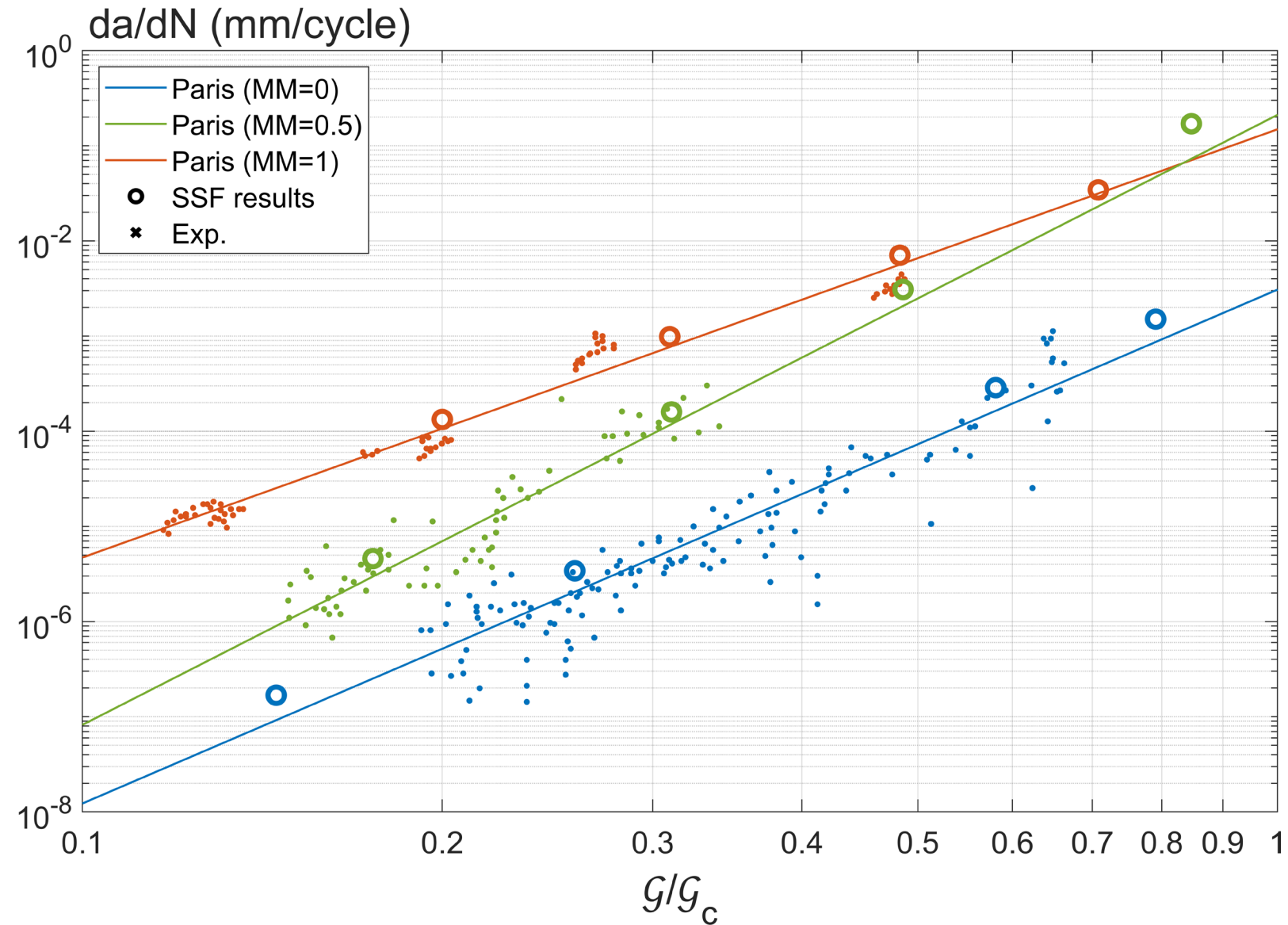
# SSF VALIDATION

Experimental data from Asp et al. (2001)



Applied moment  $\rightarrow$  Constant propagation speed

# SSF PERFORMANCE



# SSF AND DC COMPARISON

<b>Simulation</b>	<b>DC Time</b>	<b>SSF Time</b>	<b>Reduction factor</b>
<b>Finer mesh – mode I 0.5 mm propagation</b>	<b>39 h, 58 m, 54 s</b>		
<b>Coarse mesh – mode I 10 mm propagation</b>			
<b>Coarse mesh – mixed mode 10 mm propagation</b>			
<b>Coarse mesh – mode II 10 mm propagation</b>			



# SSF AND DC COMPARISON

Simulation	DC Time	SSF Time	Reduction factor
Finer mesh – mode I 0.5 mm propagation	39 h, 58 m, 54 s	2 m, 46 s	<b>867</b>
Coarse mesh – mode I 10 mm propagation	86 h, 42 m, 45 s	8 m, 29 s	<b>613</b>
Coarse mesh – mixed mode 10 mm propagation	76 h, 3 m, 15 s	9 m, 46 s	<b>305</b>
Coarse mesh – mode II 10 mm propagation	52 h, 43 m, 48 s	14 m, 56 s	<b>212</b>

# BENCHMARK VALIDATION

Composite Structures 210 (2019) 932–941

Contents lists available at [ScienceDirect](https://www.sciencedirect.com)

Composite Structures

journal homepage: [www.elsevier.com/locate/compstruct](http://www.elsevier.com/locate/compstruct)



ELSEVIER



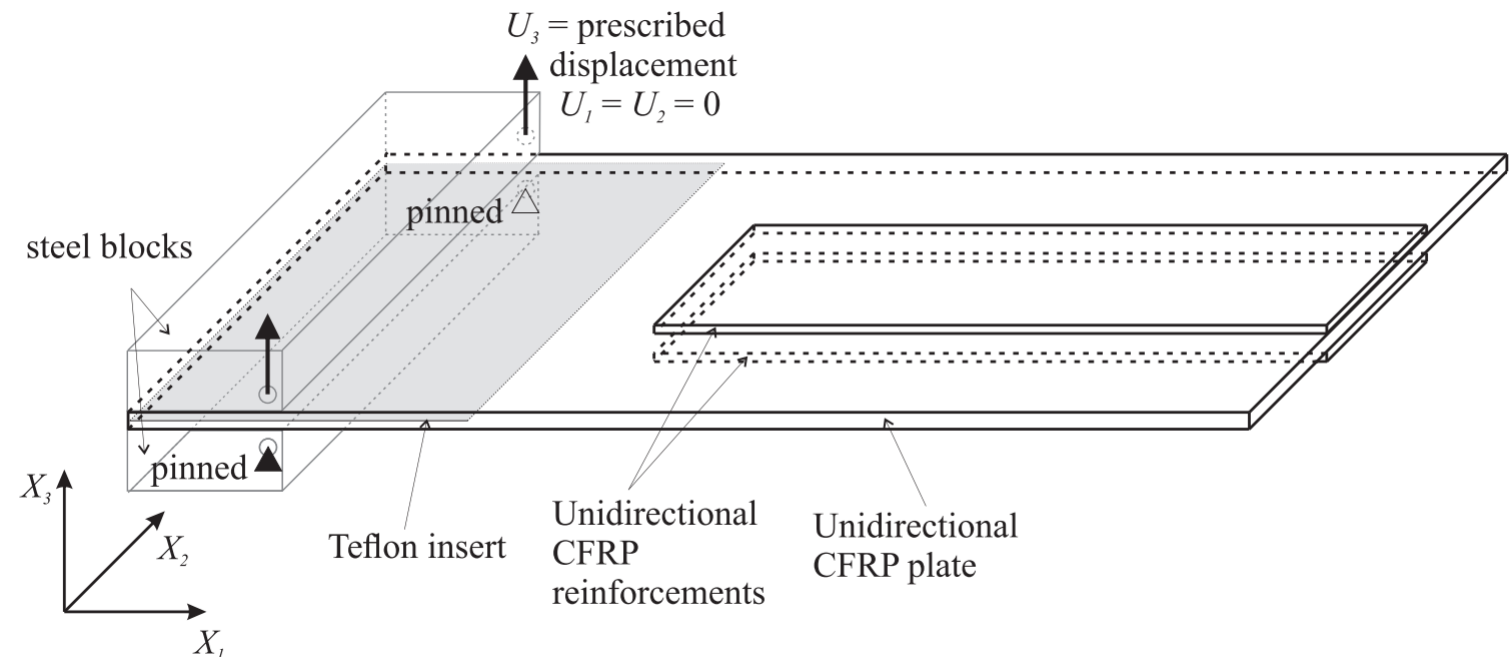
## A benchmark test for validating 3D simulation methods for delamination growth under quasi-static and fatigue loading

L. Carreras<sup>a,\*</sup>, J. Renart<sup>a</sup>, A. Turon<sup>a</sup>, J. Costa<sup>a</sup>, B.L.V. Bak<sup>b</sup>, E. Linares<sup>c</sup>,  
F. Martin de la Escalera<sup>c</sup>, Y. Essa<sup>c</sup>

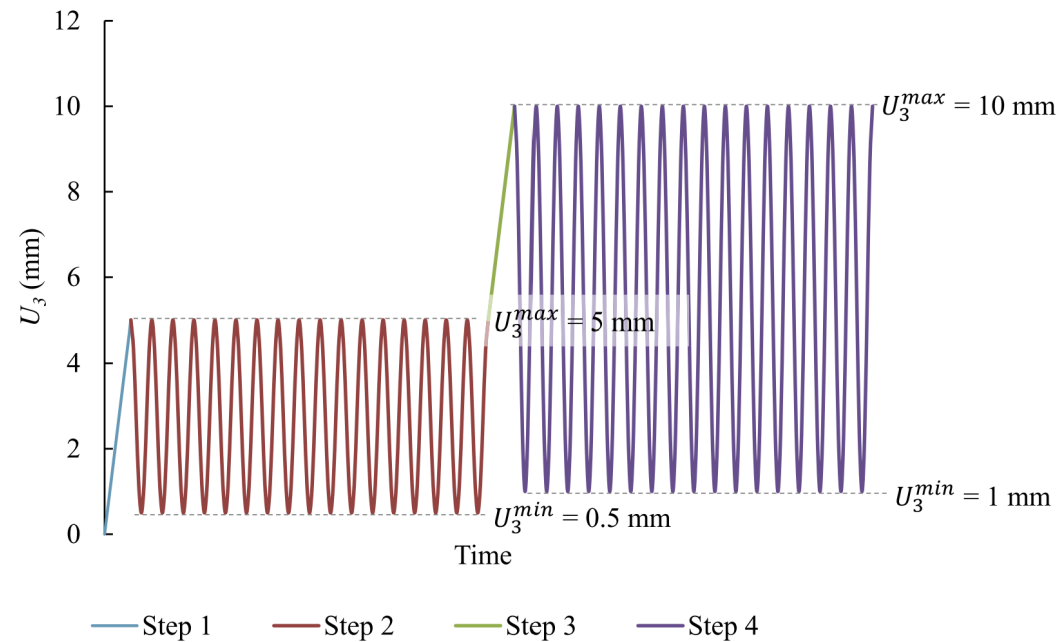
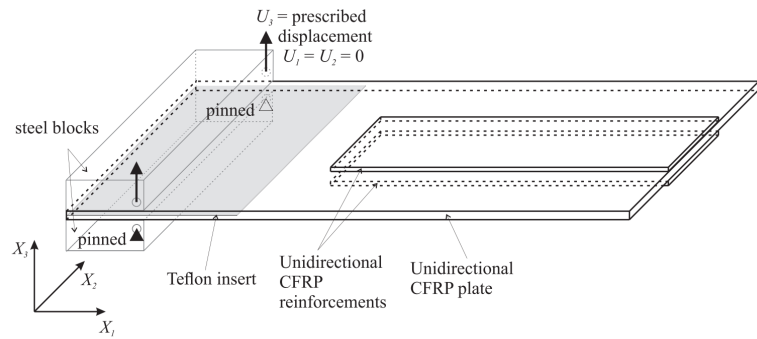
<sup>a</sup> AMADE, Polytechnic School, University of Girona, Universitat de Girona 4, E-17003 Girona, Spain

<sup>b</sup> Dept. of Materials and Production, Aalborg University, Fibigerstraede 16, DK-9220 Aalborg East, Denmark

<sup>c</sup> AERNNOVA Engineering Division SA, Llano Castellano Avenue 13, E-28034 Madrid, Spain

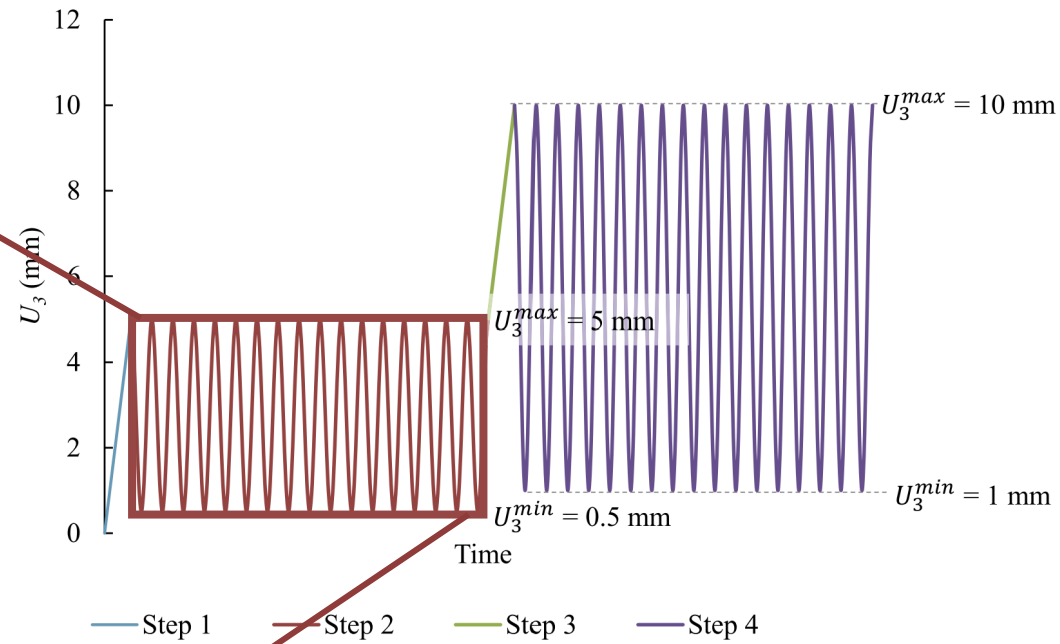
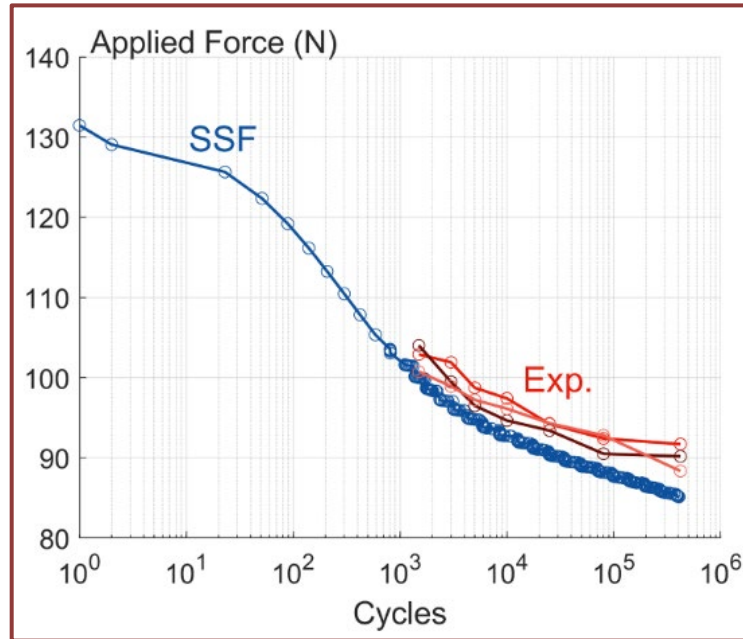
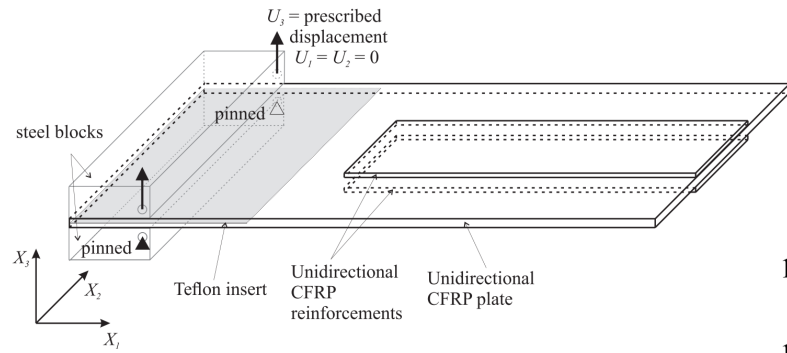


# BENCHMARK VALIDATION

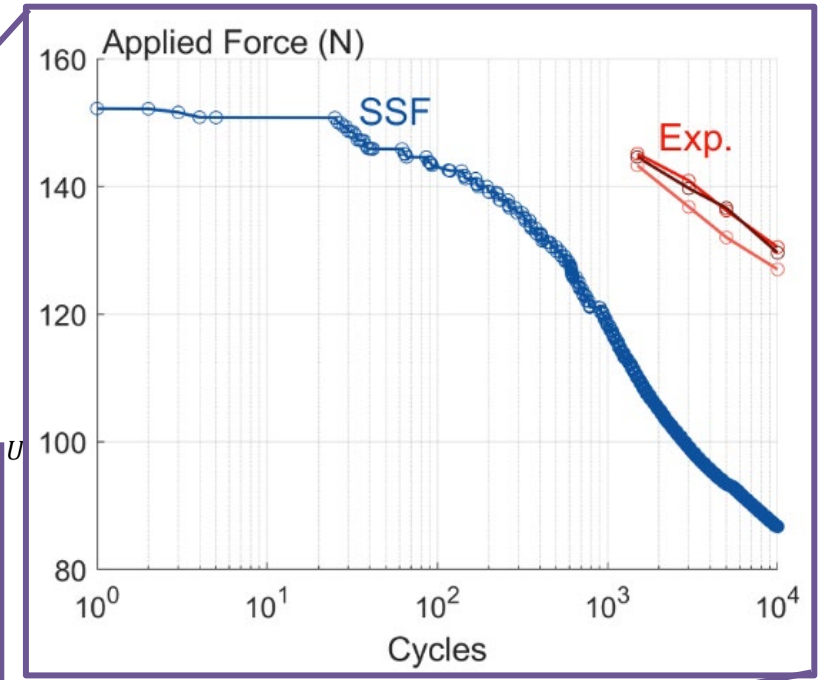
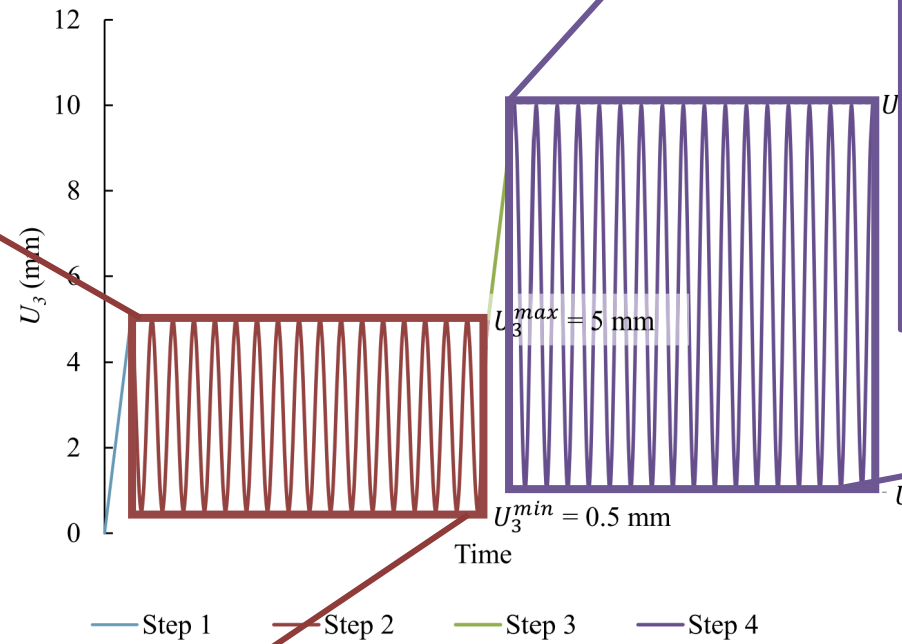
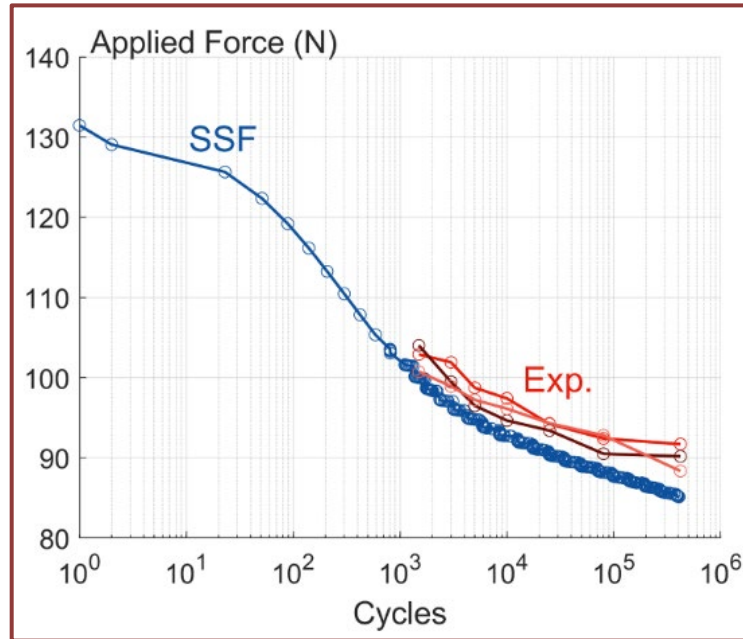
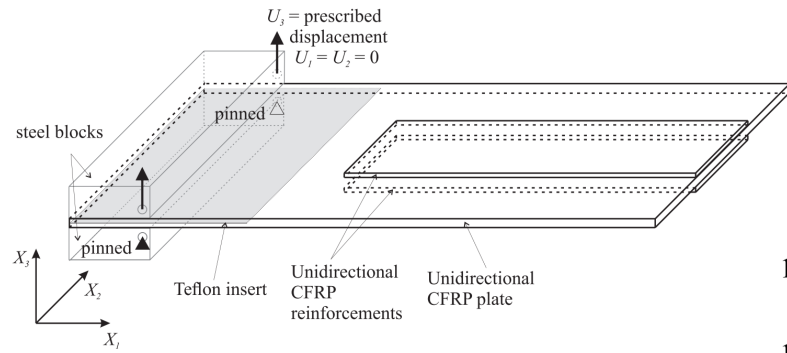




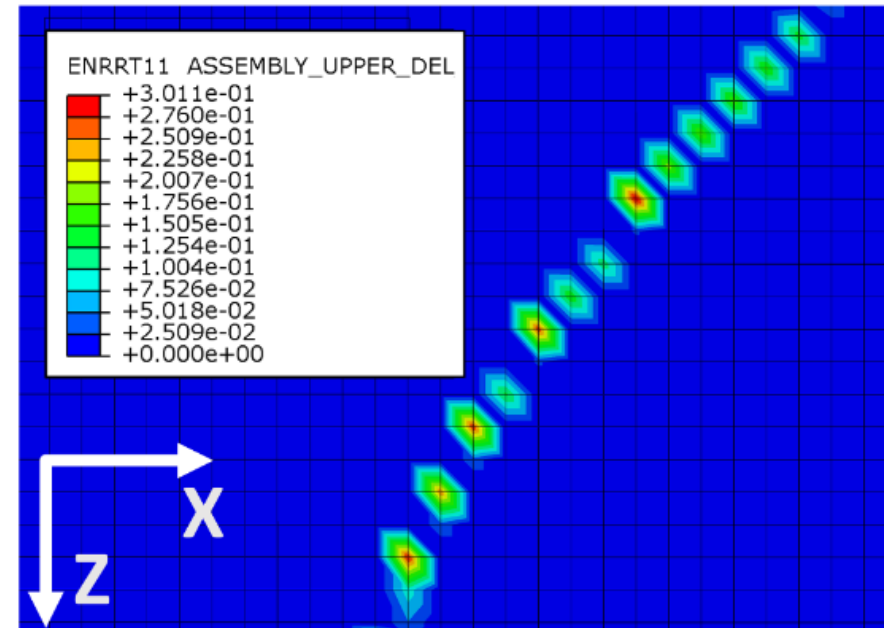
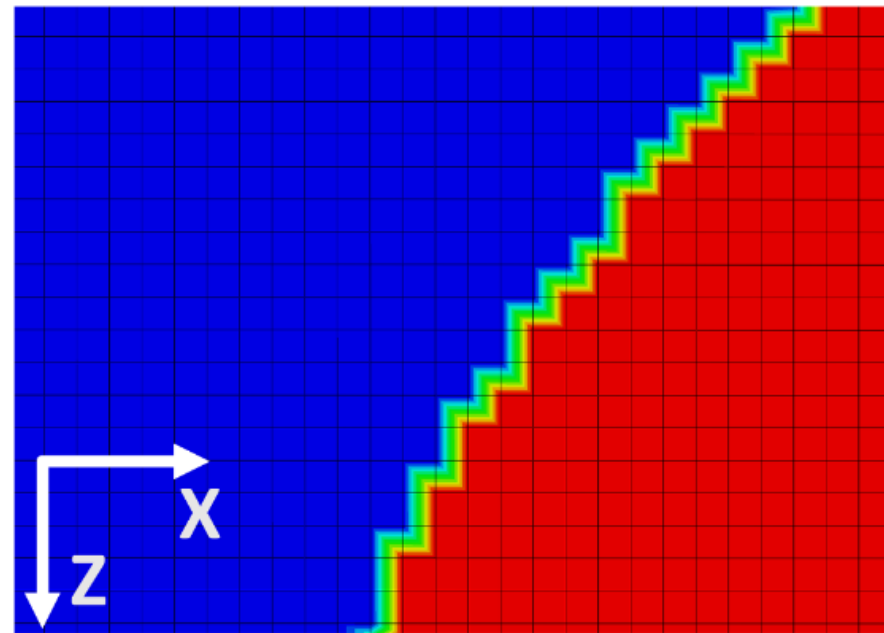
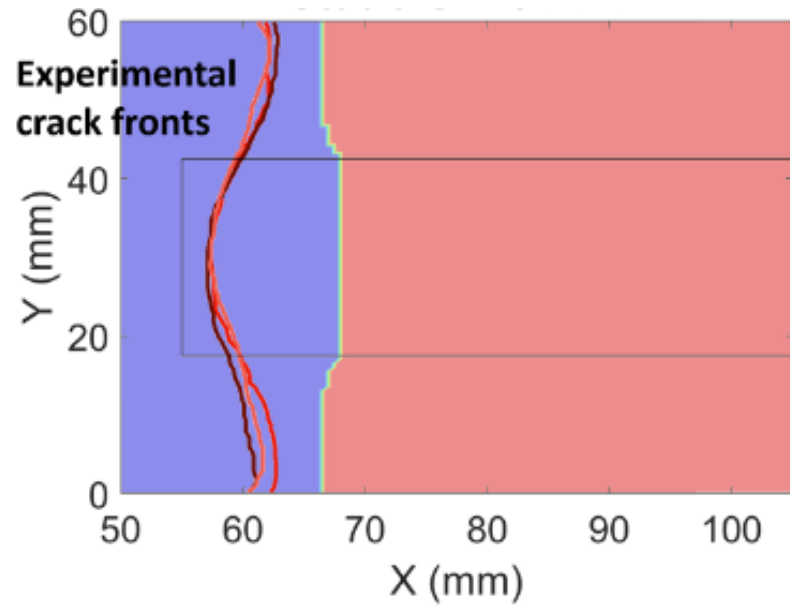
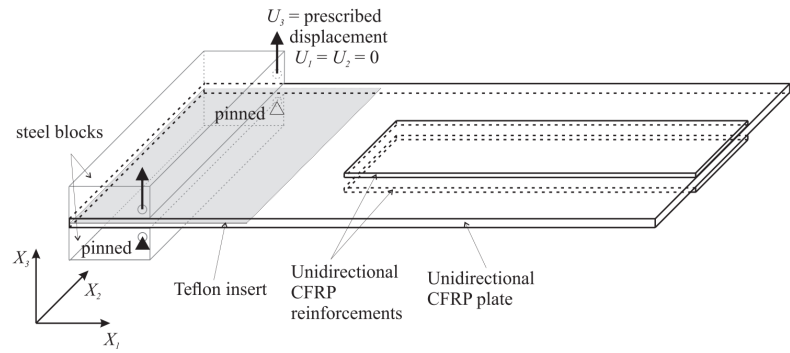
# BENCHMARK VALIDATION



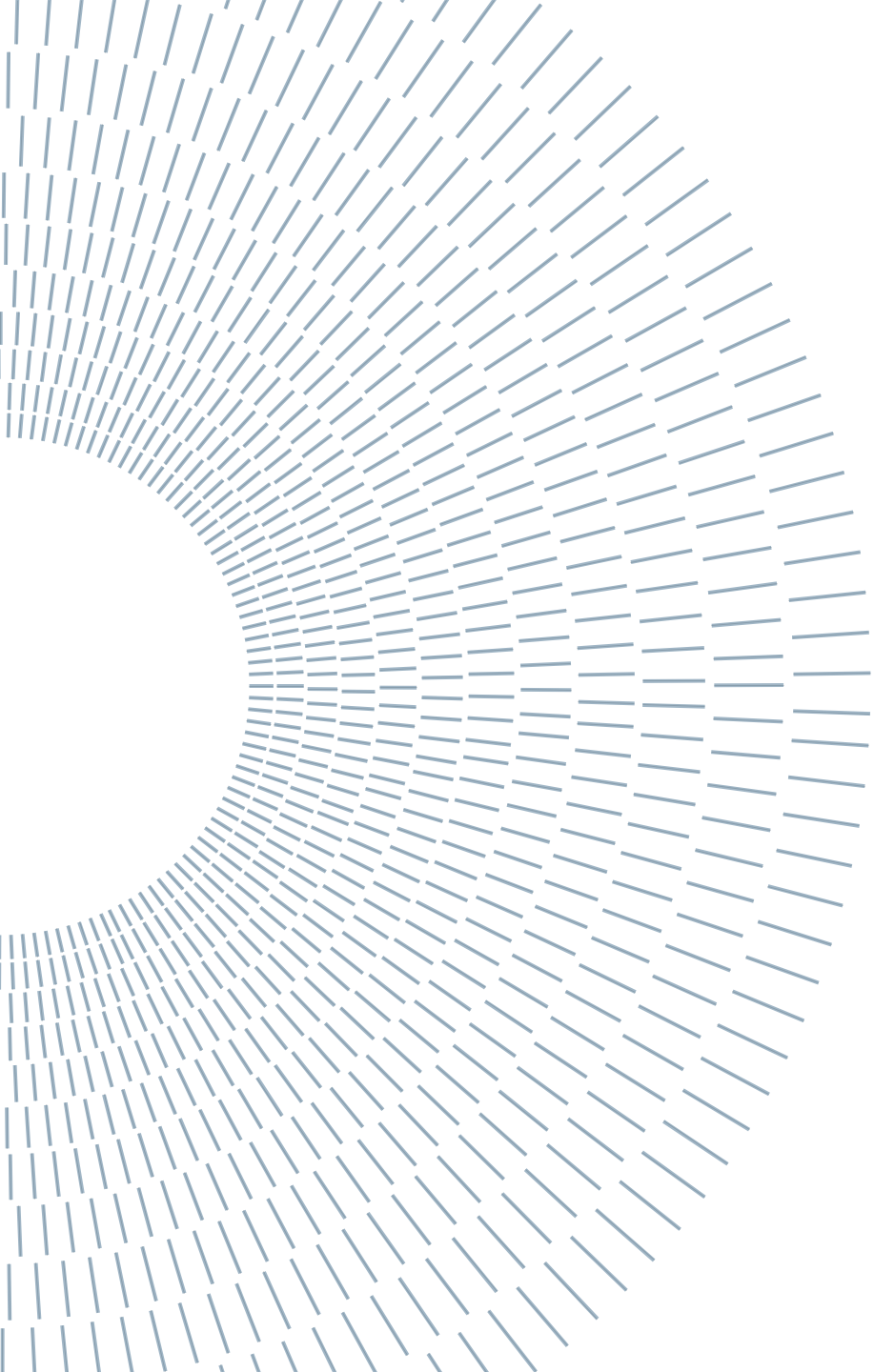
# BENCHMARK VALIDATION



# PROBLEMS

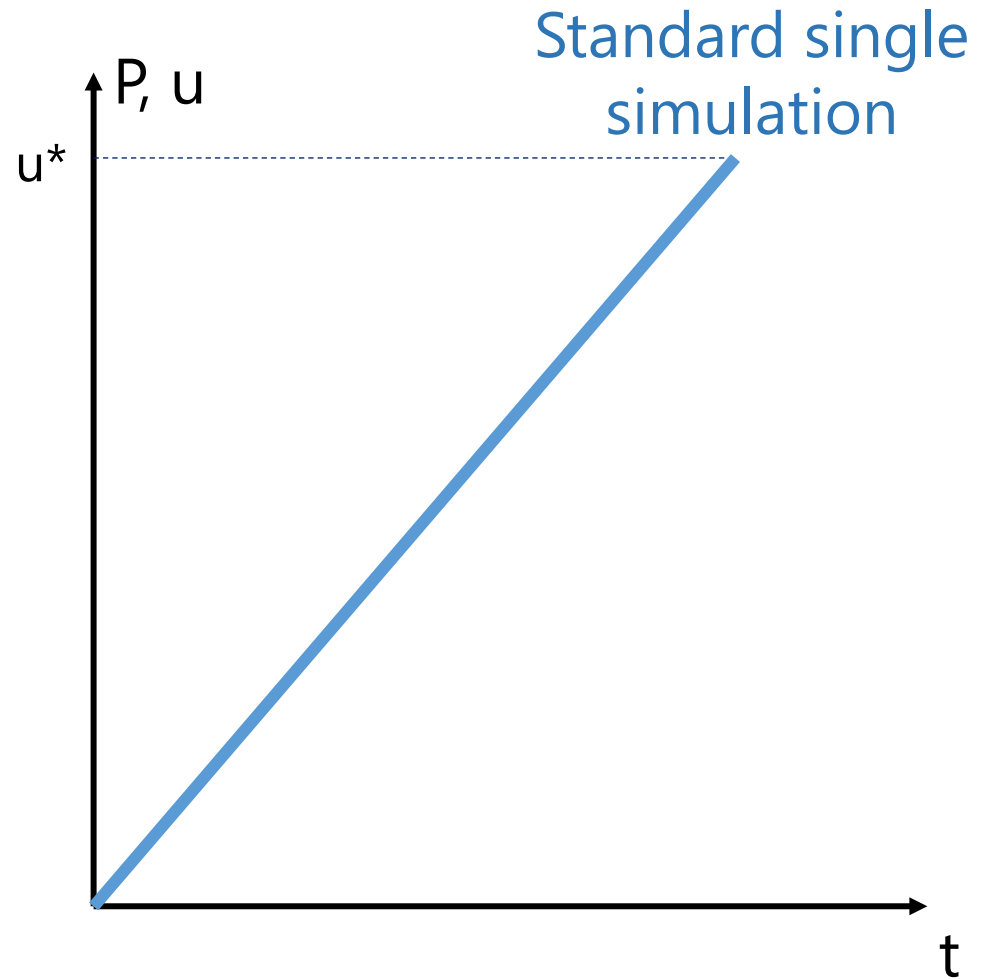




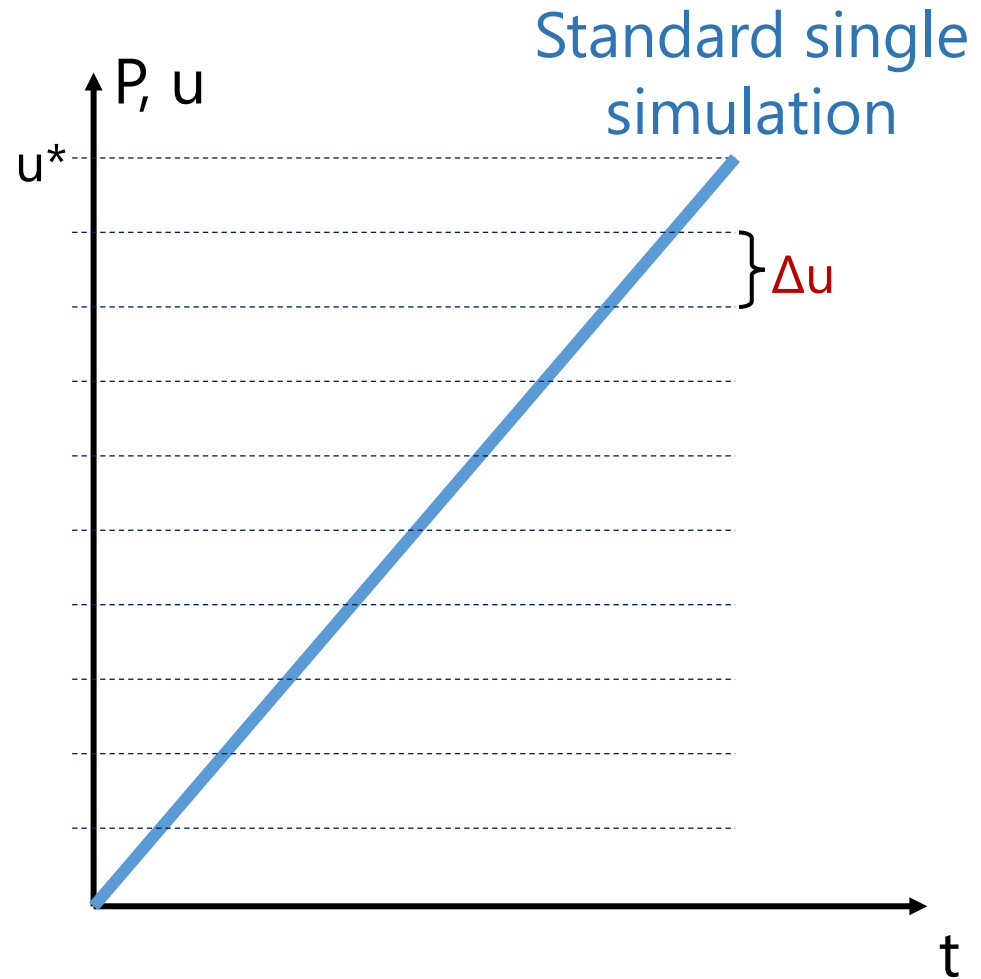


# **SIMULATIONS OF DELAMINATIONS UNDER STATIC LOADINGS**

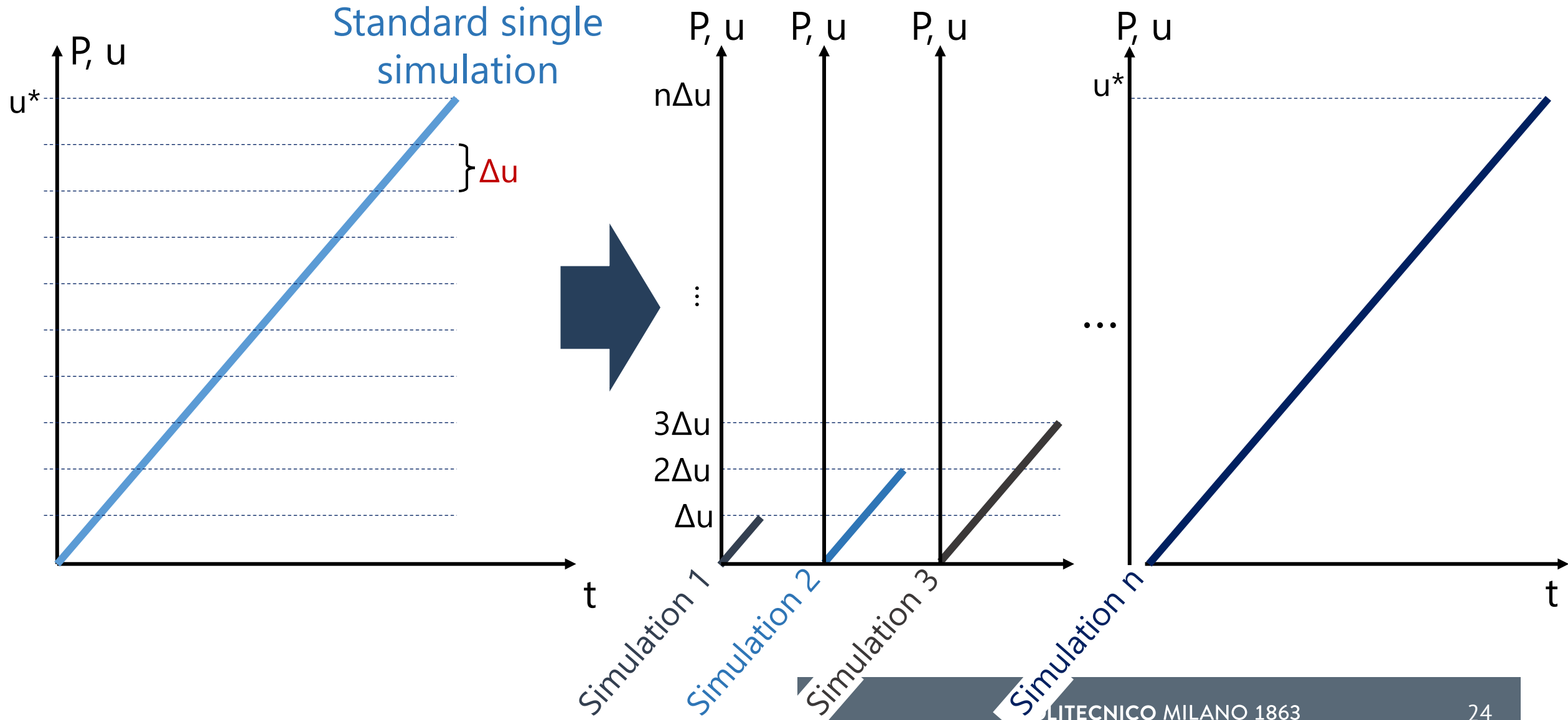
# STATIC SEQUENTIAL ALGORITHM



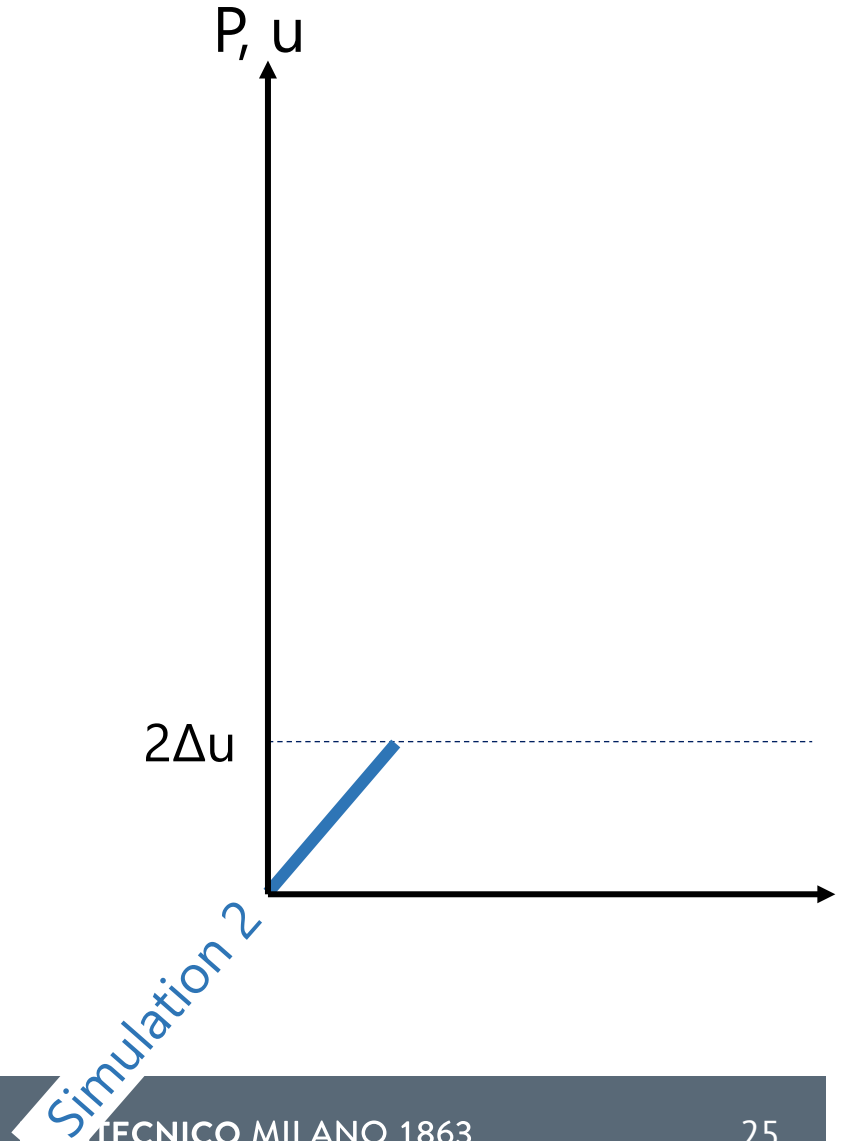
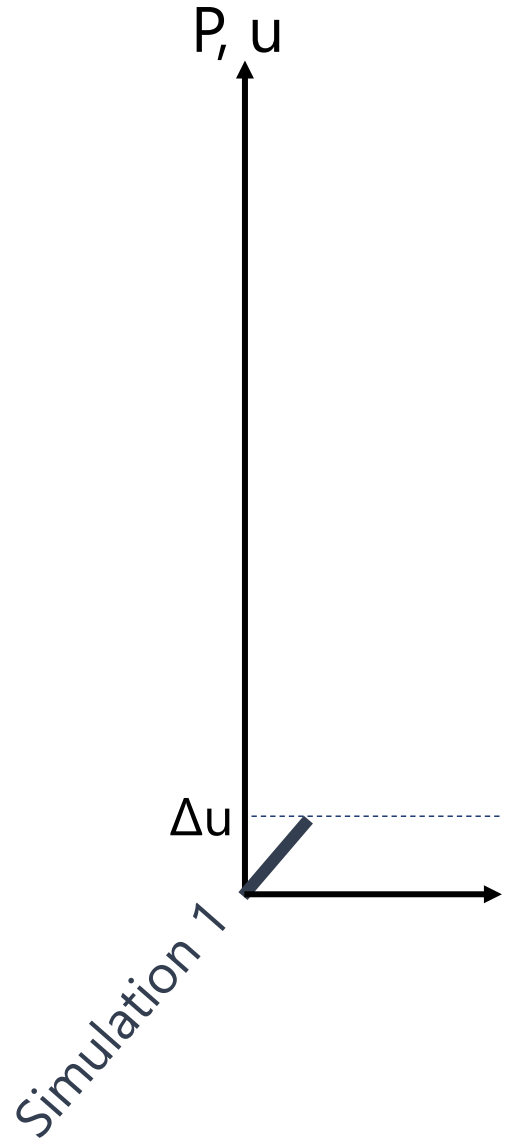
# STATIC SEQUENTIAL ALGORITHM



# STATIC SEQUENTIAL ALGORITHM

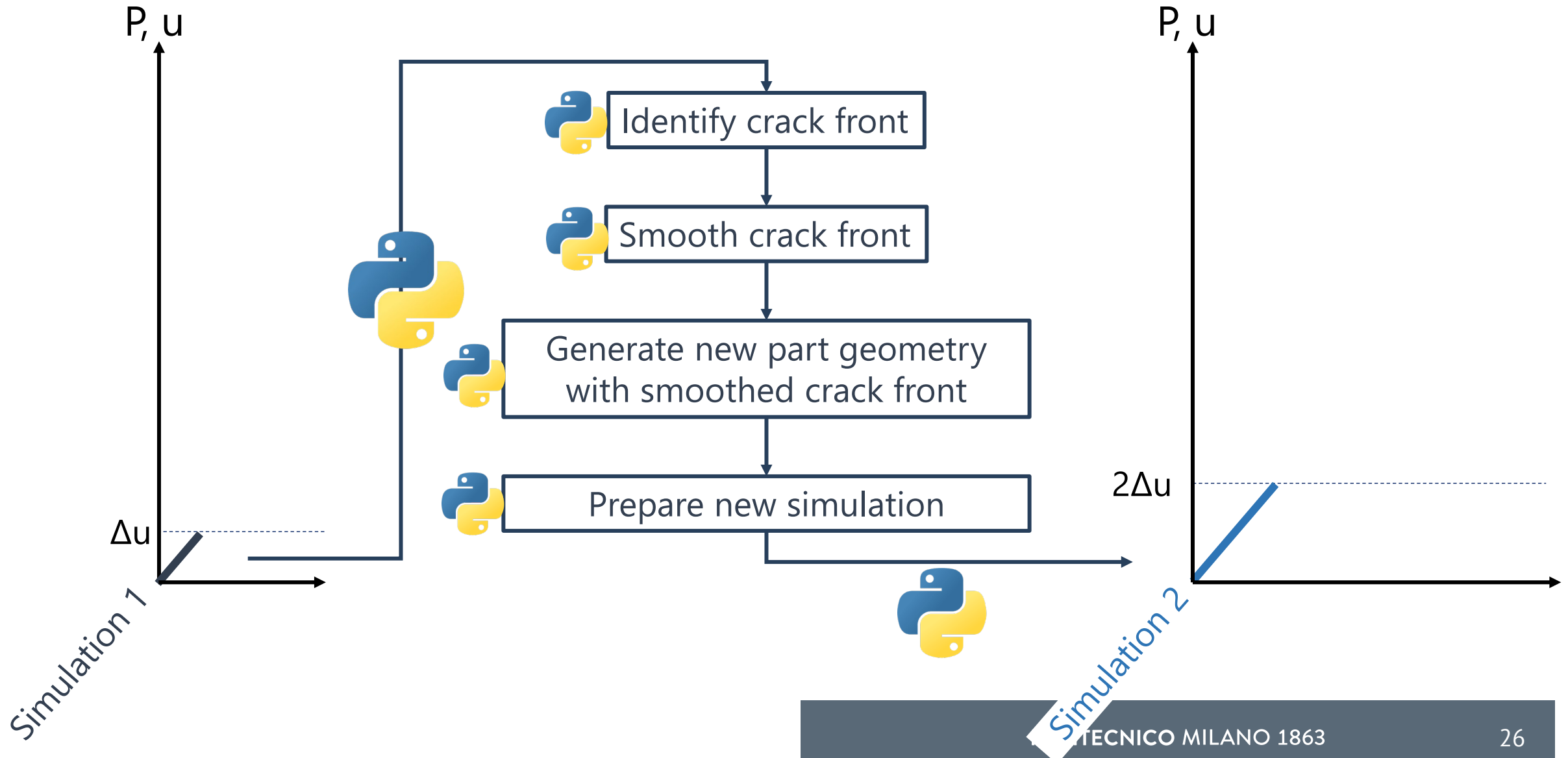


# STATIC SEQUENTIAL ALGORITHM

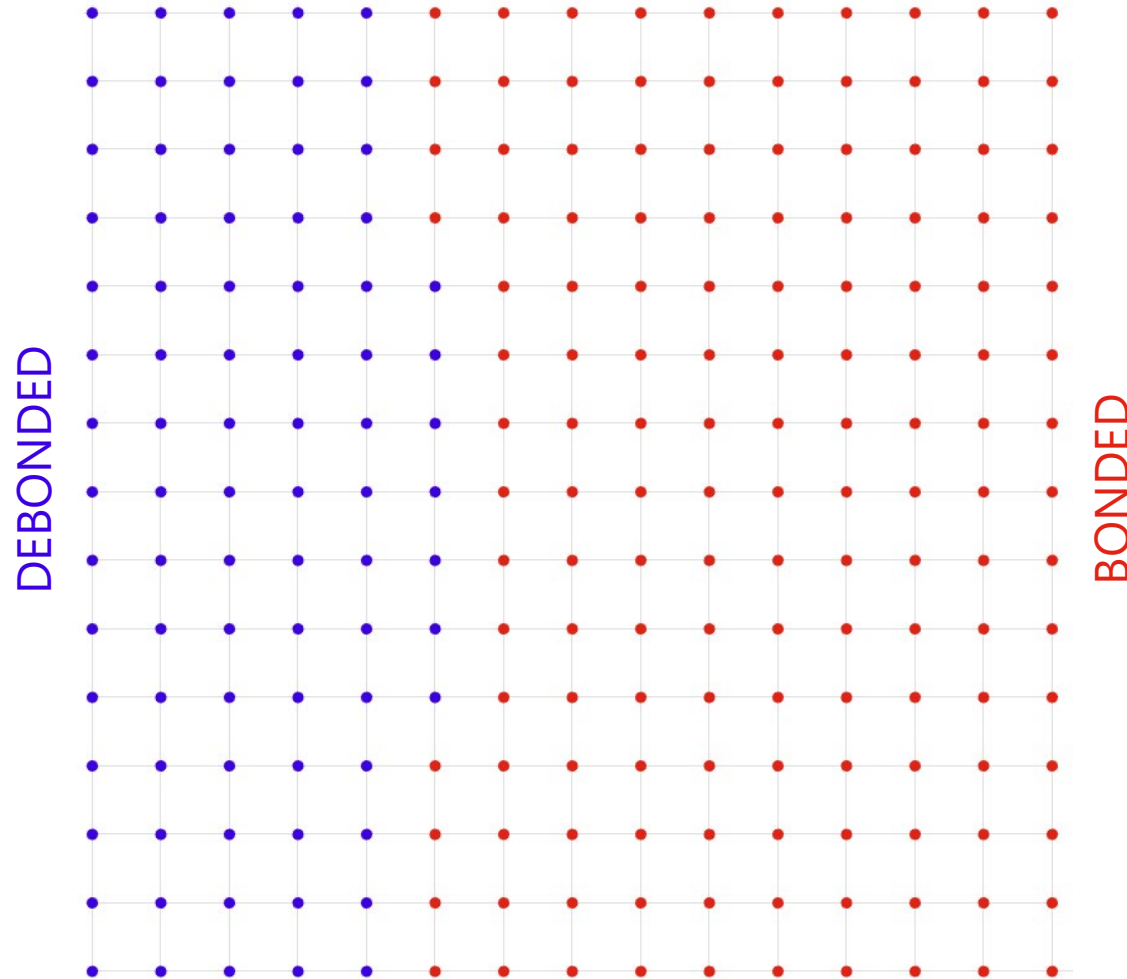




# STATIC SEQUENTIAL ALGORITHM

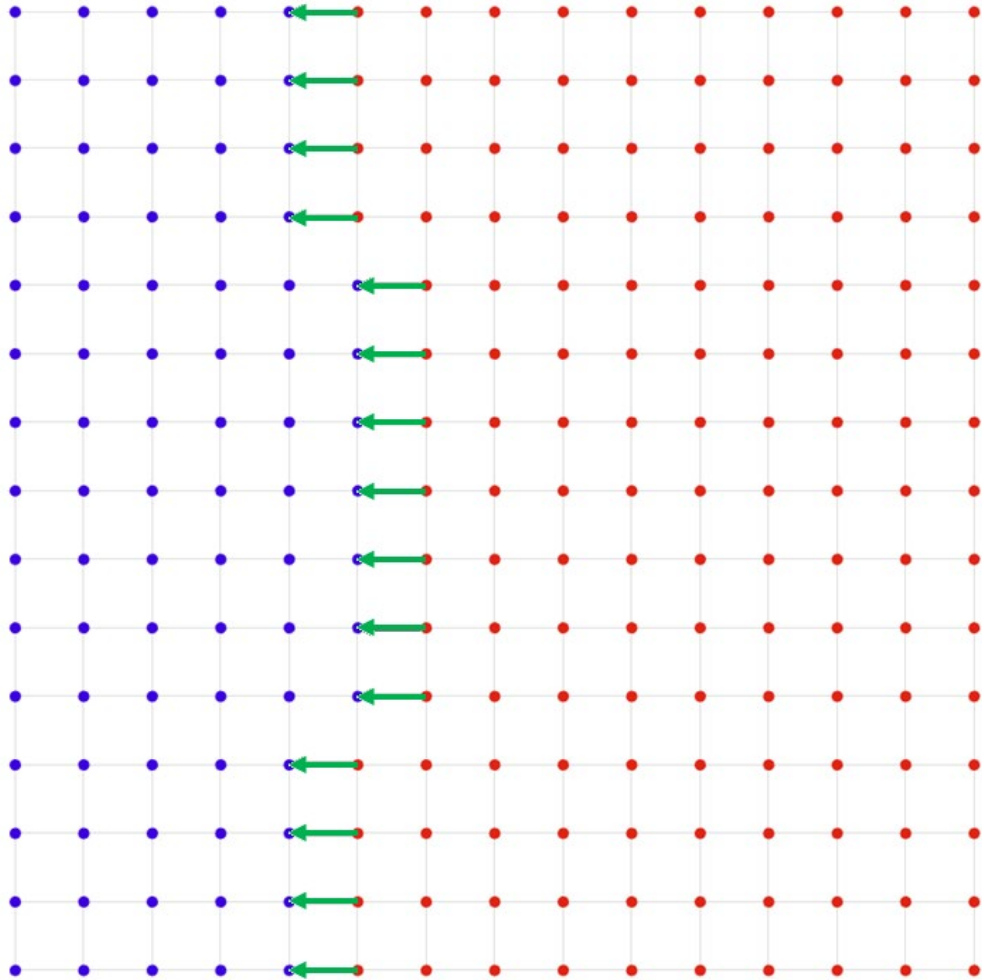


# FRONT IDENTIFICATION



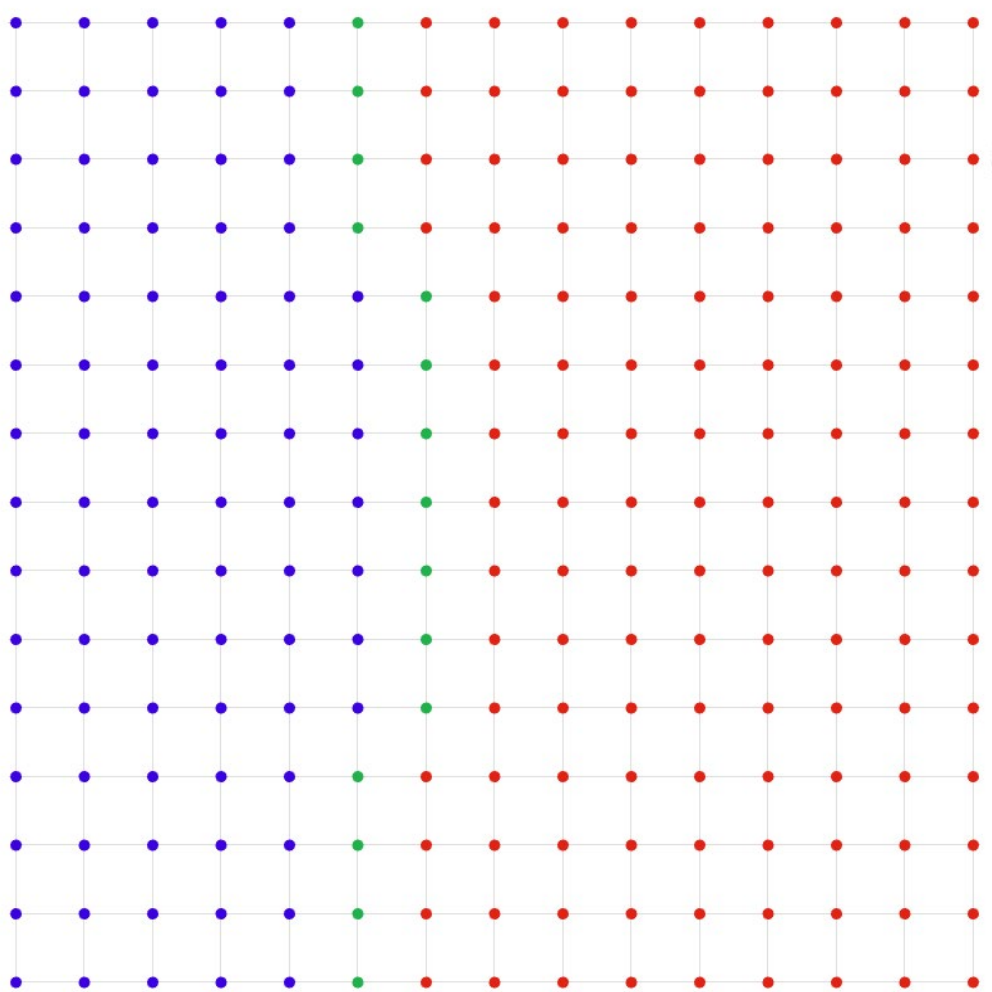
The Abaqus model does not define the delamination front. It uses bonded (red) and de-bonded (blue) nodes.

# FRONT IDENTIFICATION



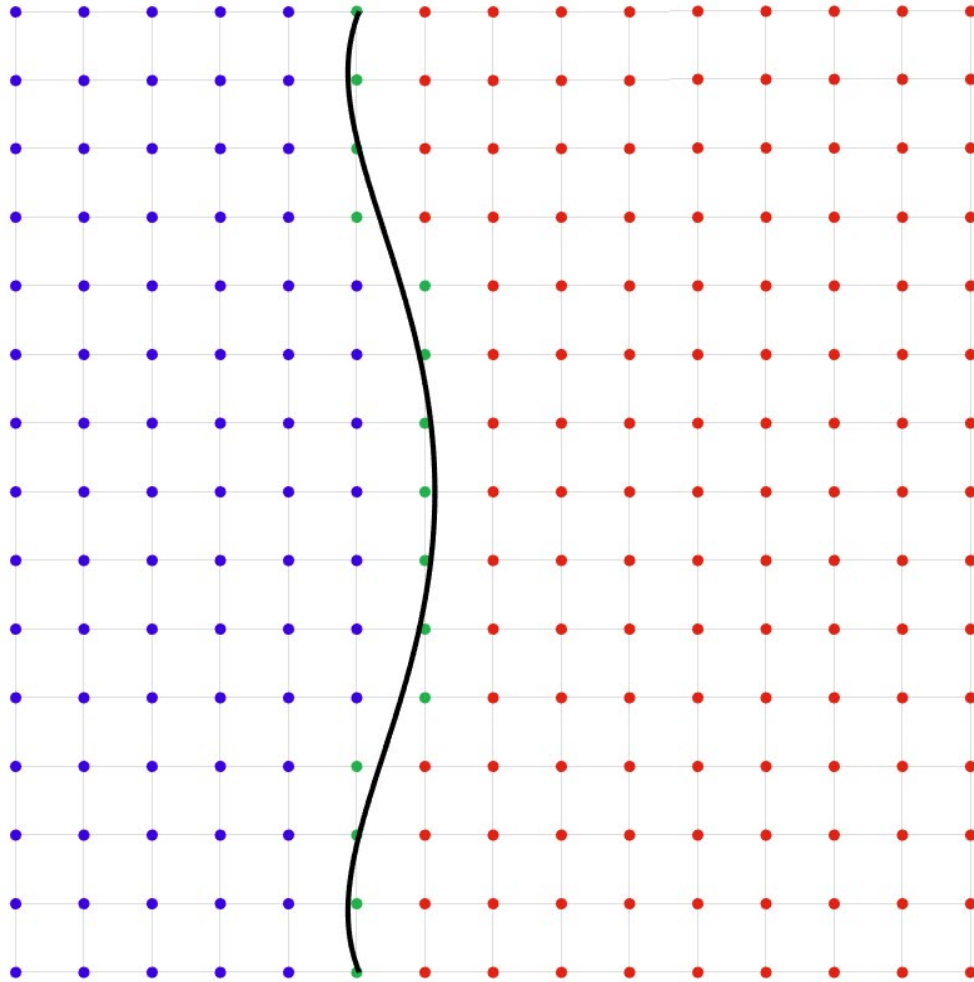
The front is identified using the distance between bonded and de-bonded nodes.

# FRONT IDENTIFICATION



If the distance is under a threshold proportional to the element size, the bonded node is considered a front node.

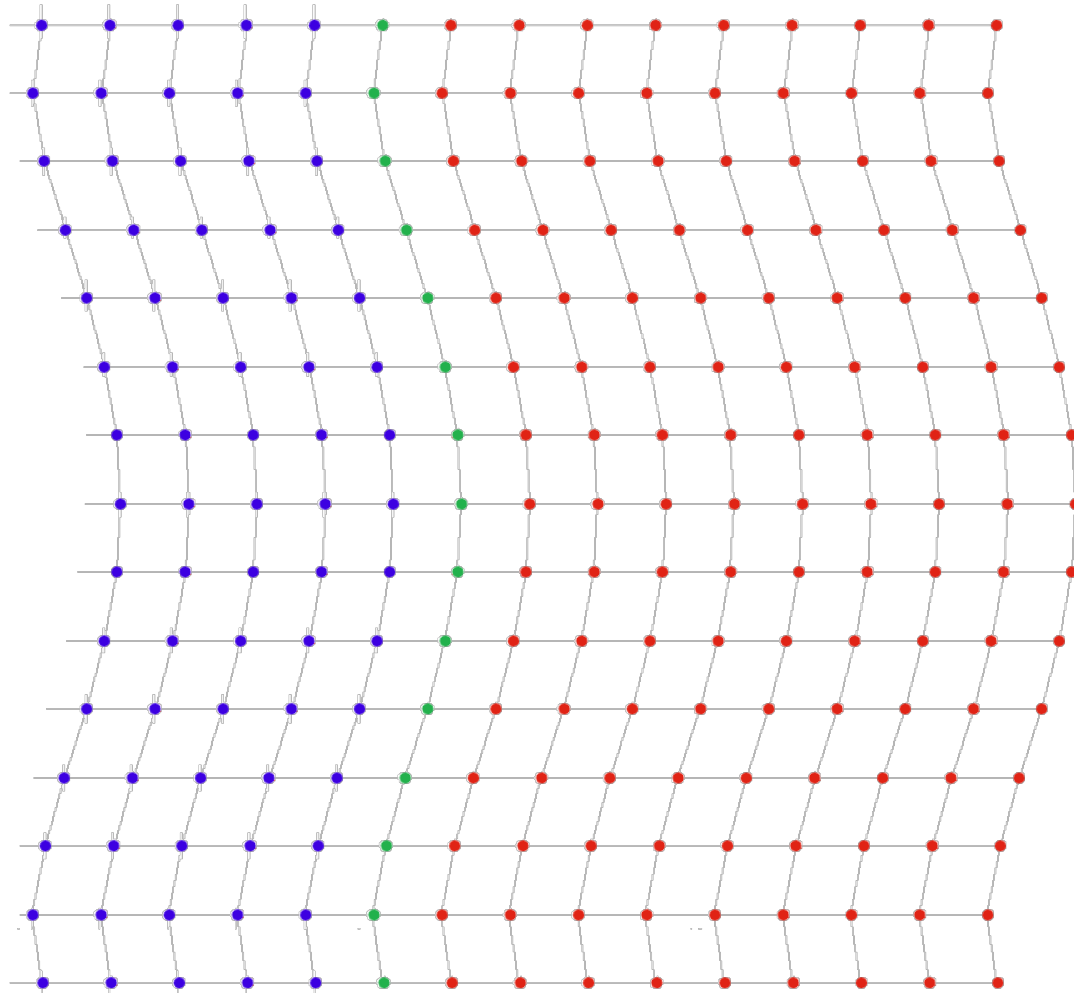
# FRONT IDENTIFICATION



The front nodes are approximated with a polynomial function.

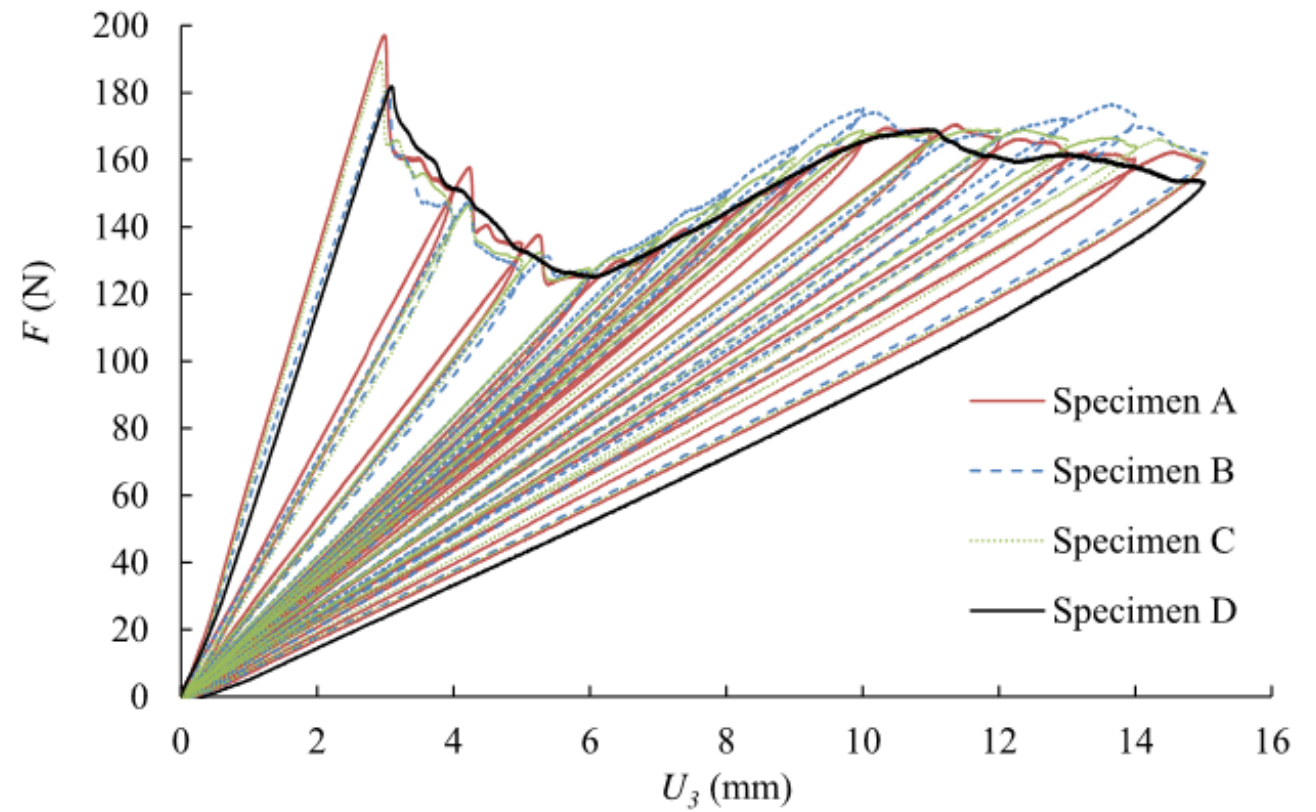
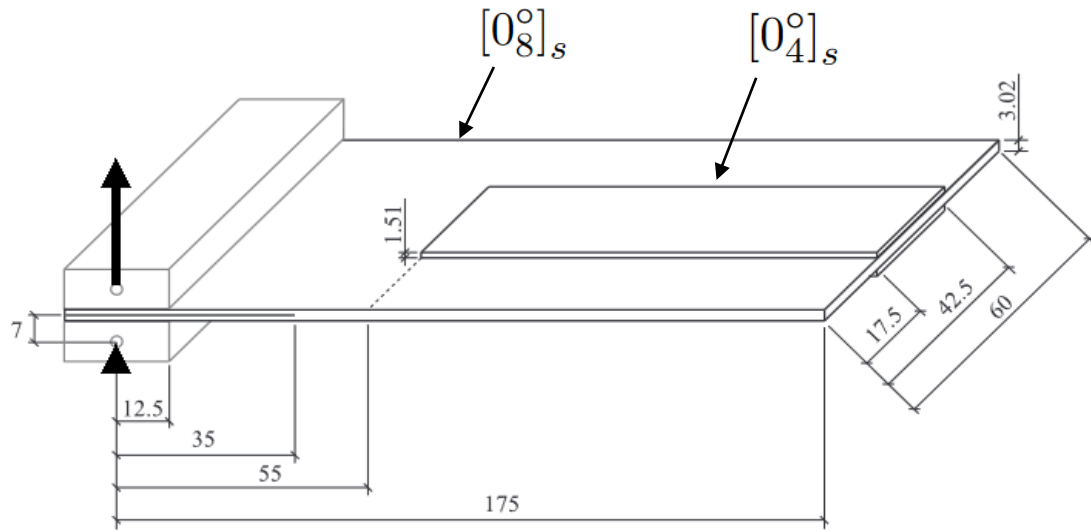


# FRONT IDENTIFICATION



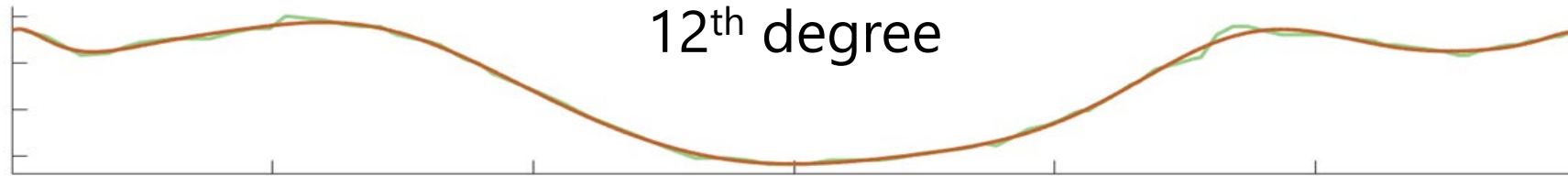
The original model is copied, partitioned along the front and remeshed.

# EXPERIMENTAL VALIDATION CASE

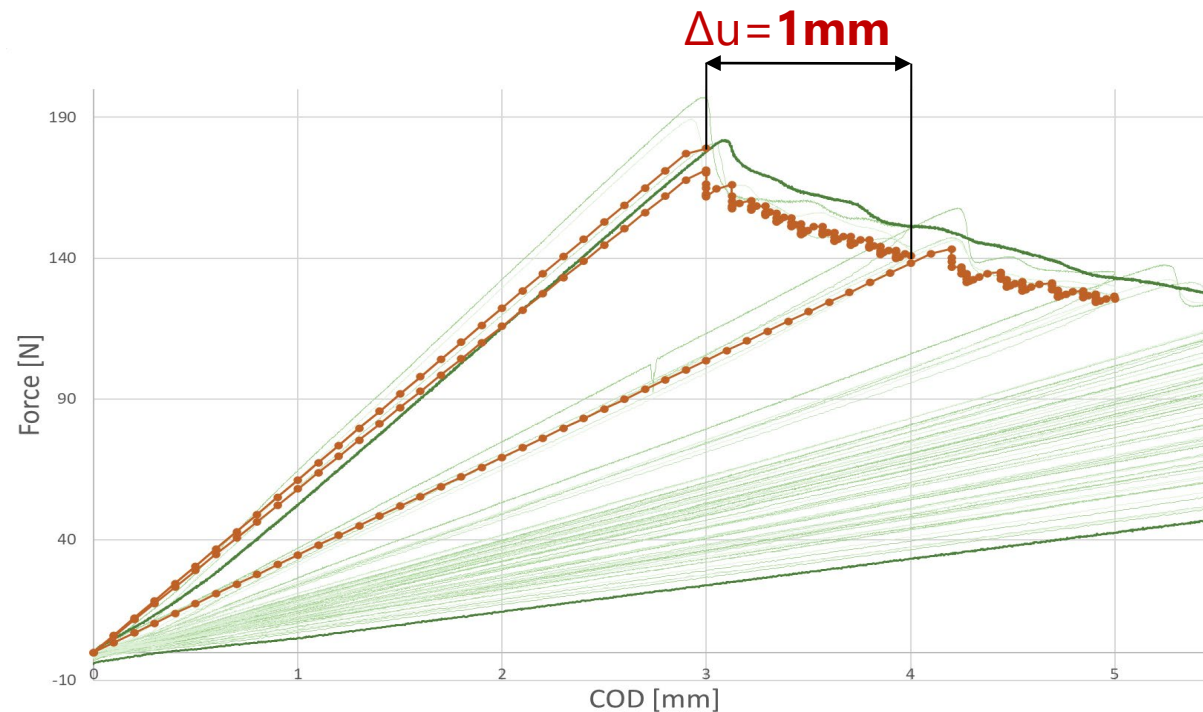


# ALGORITHM PARAMETERS

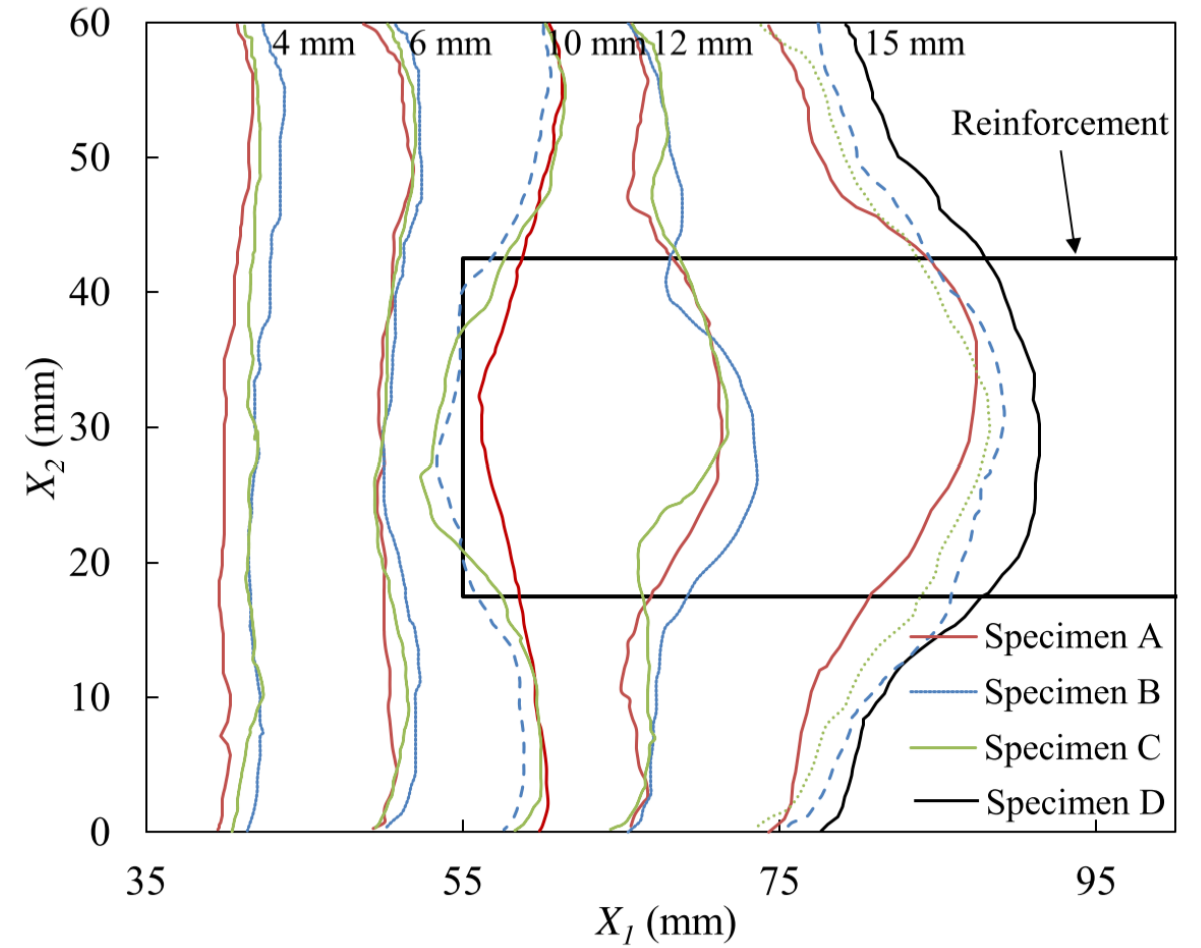
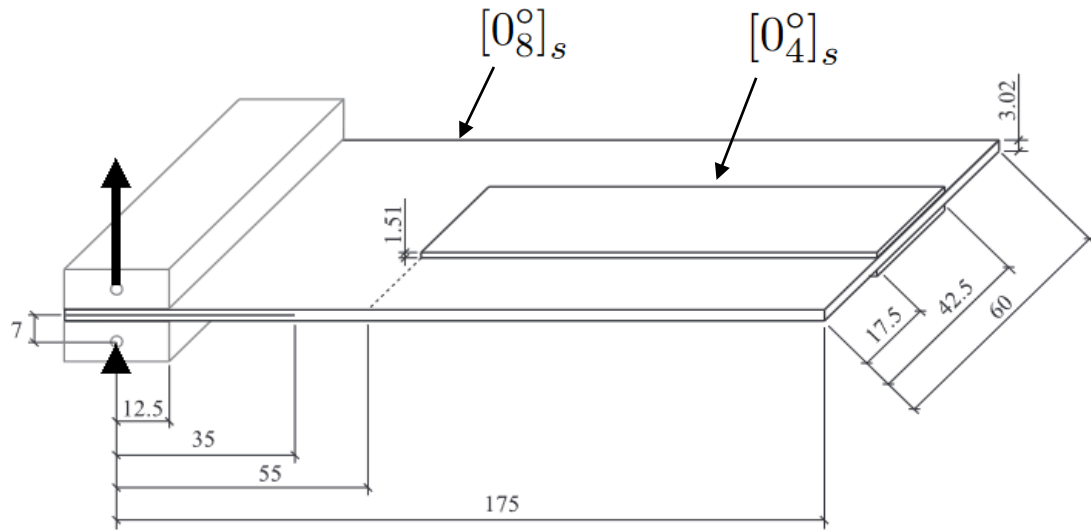
## Polynomial smoothing of crack fronts



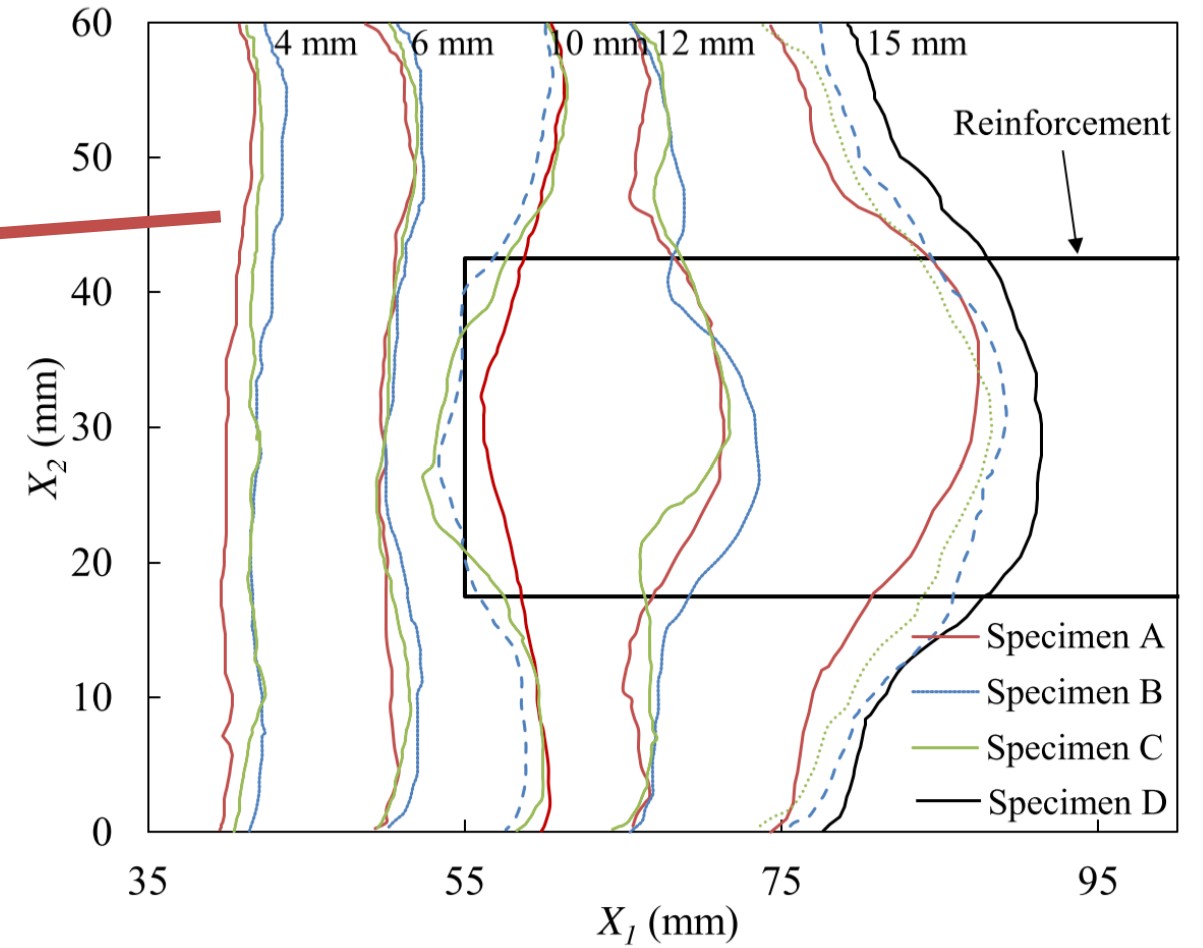
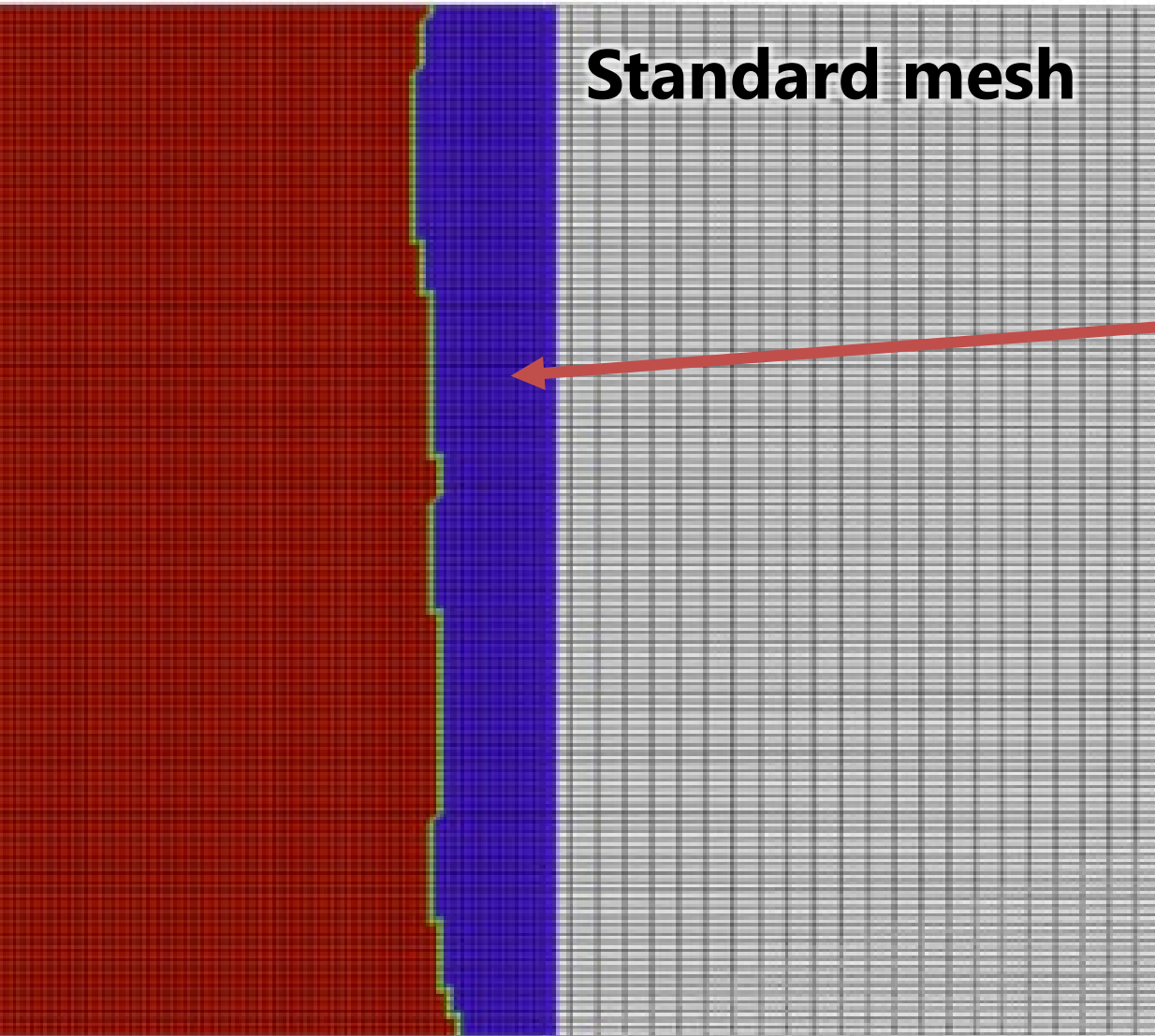
## Displacement intervals between simulations



# FIRST VALIDATION: NO PROPAGATION

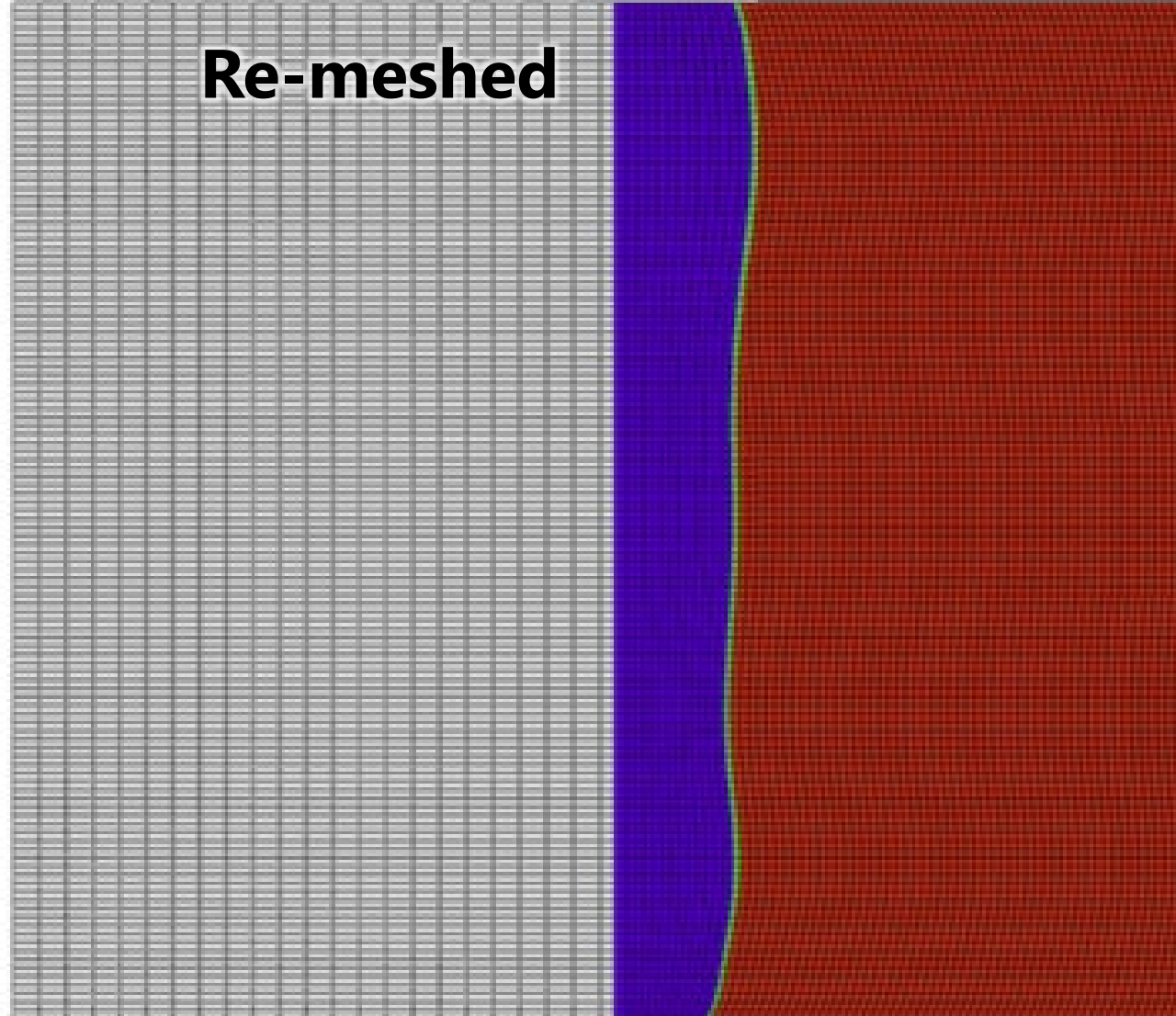
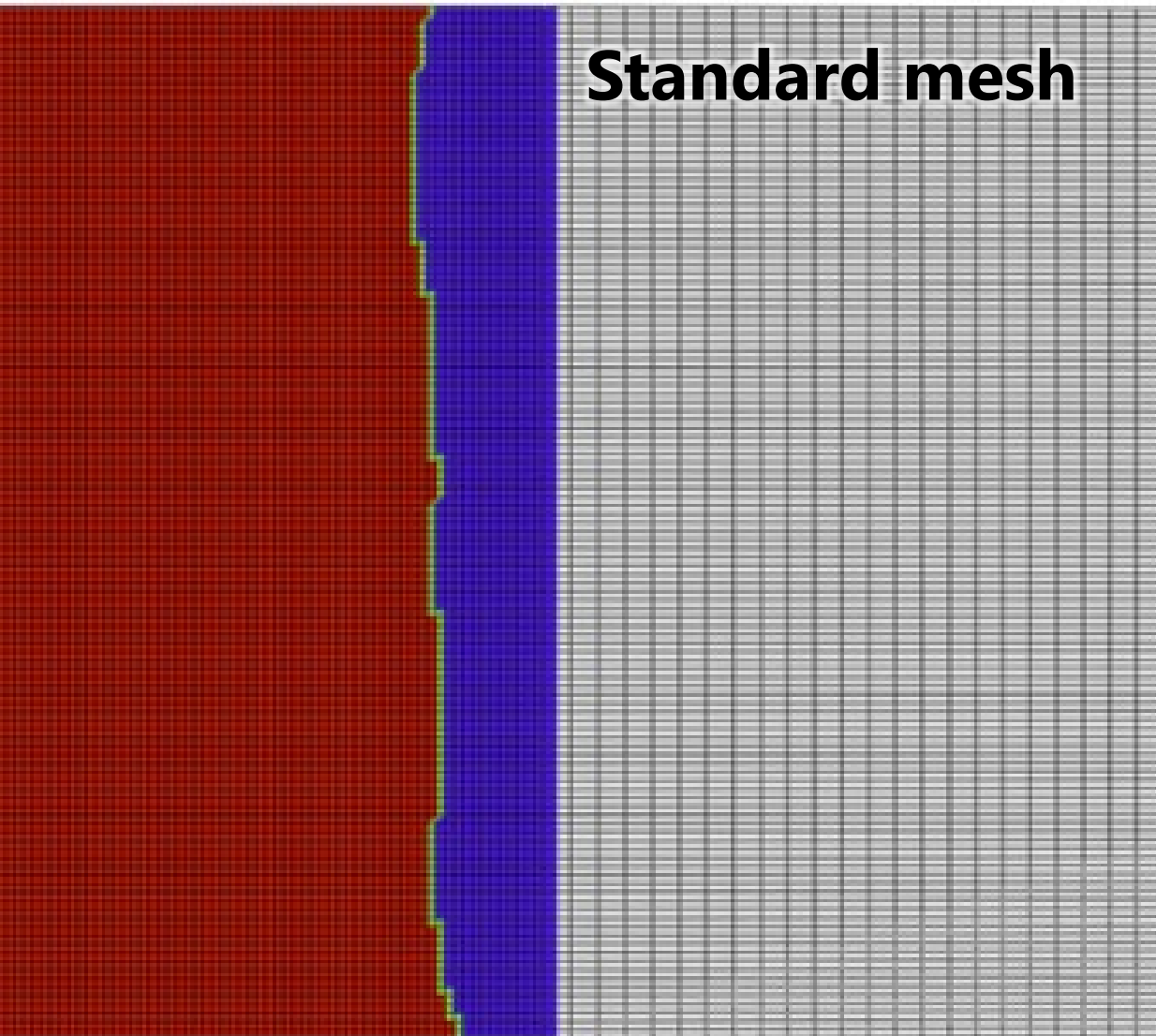


# FIRST VALIDATION: NO PROPAGATION

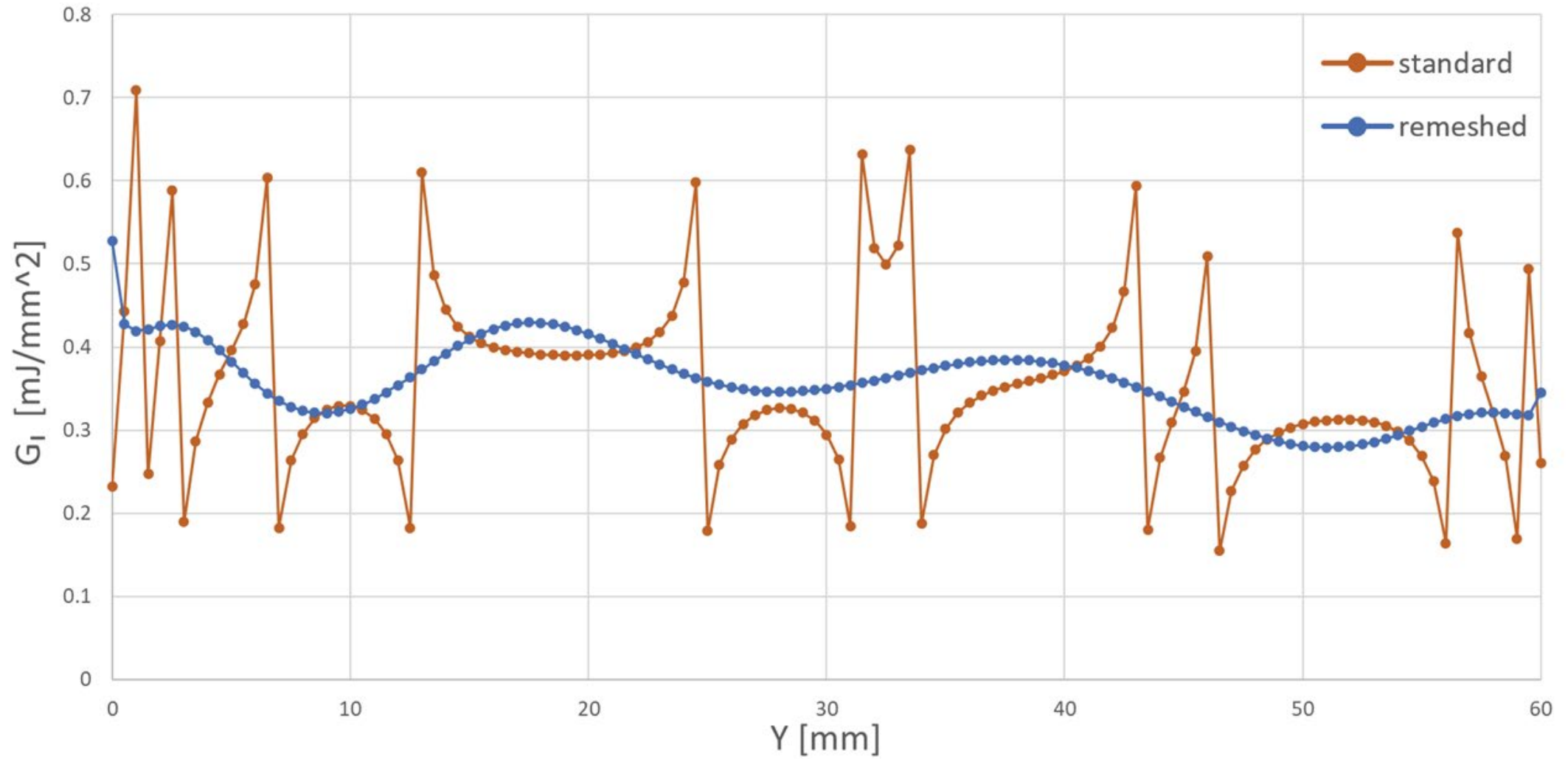




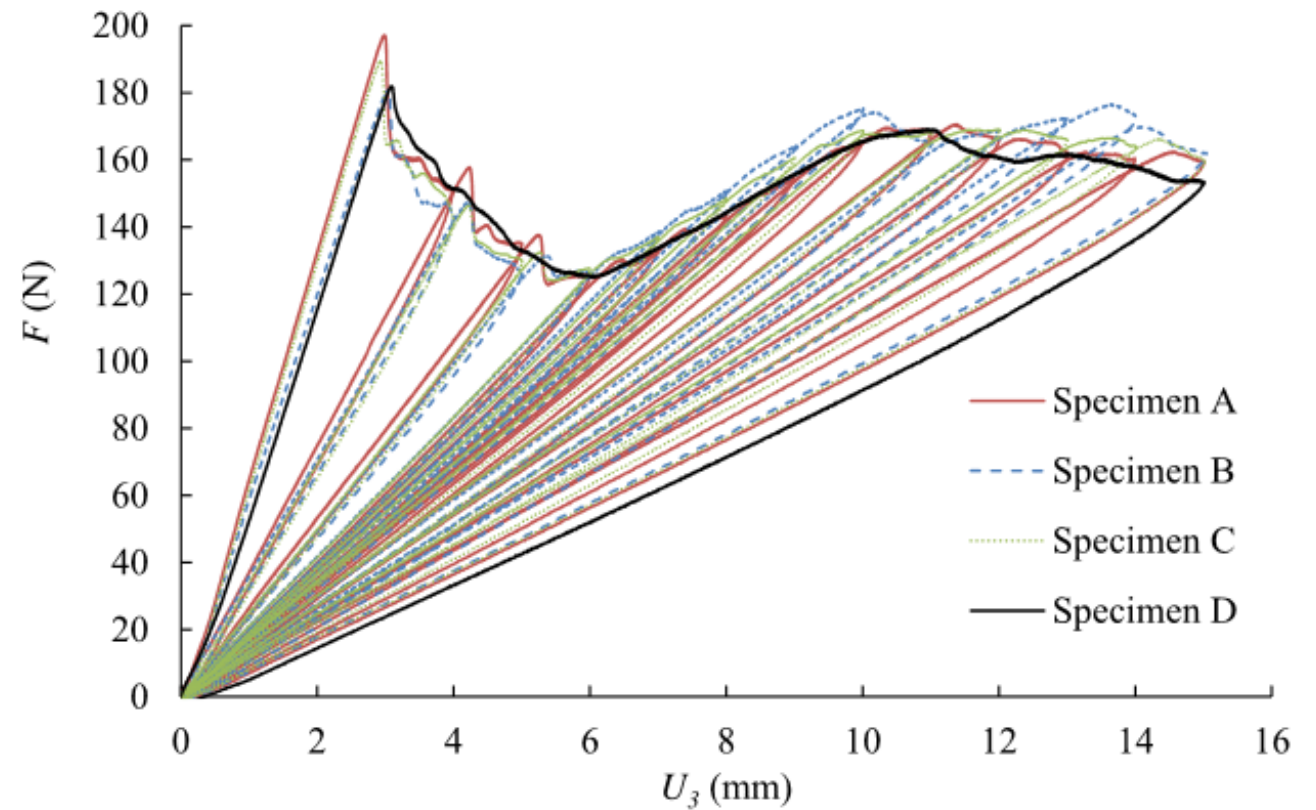
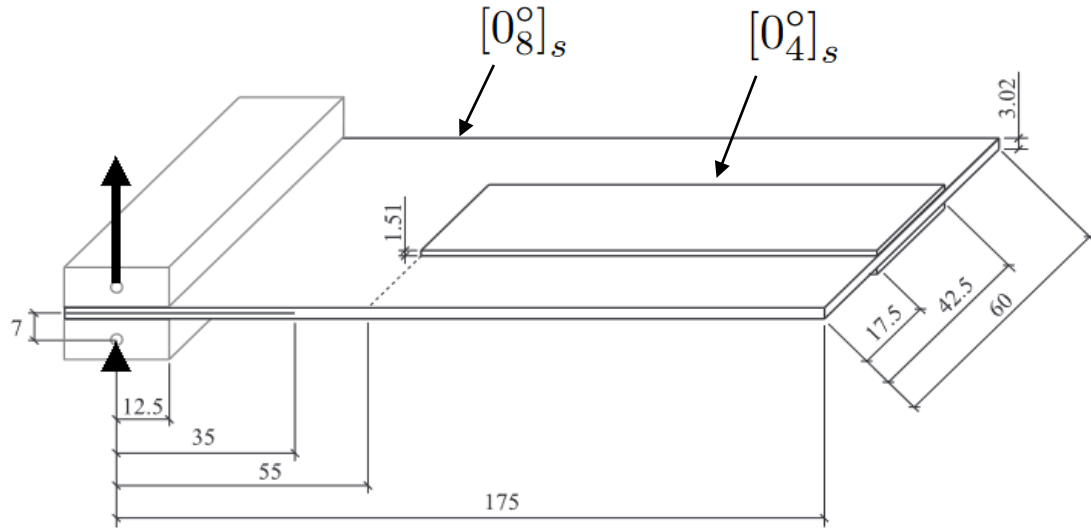
# FIRST VALIDATION: NO PROPAGATION



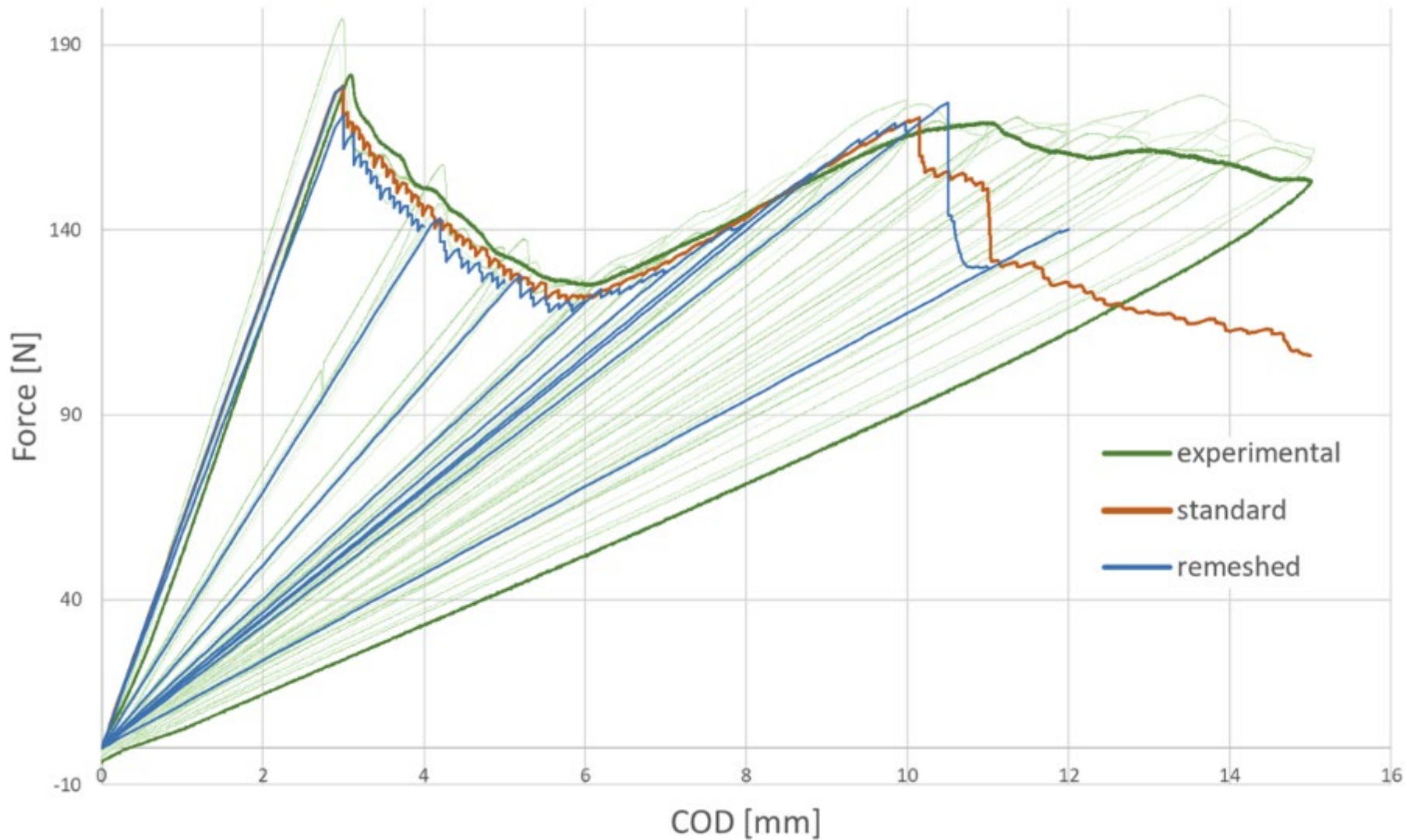
# SIMULATION WITHOUT PROPAGATION



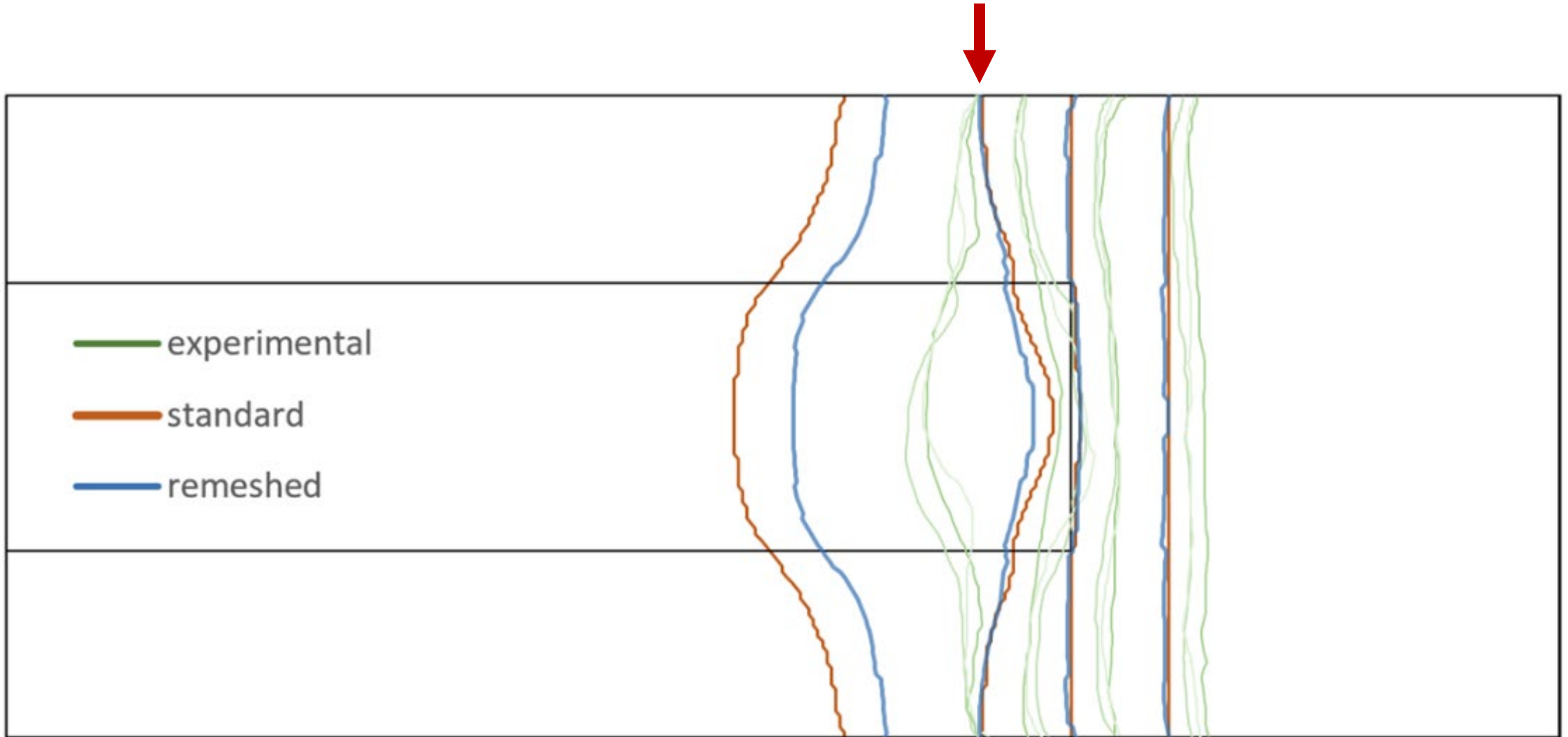
# SECOND VALIDATION: FULL SIMULATION



# BOTH TECHNIQUES UNDERESTIMATE THE DELAMINATION RESISTANCE



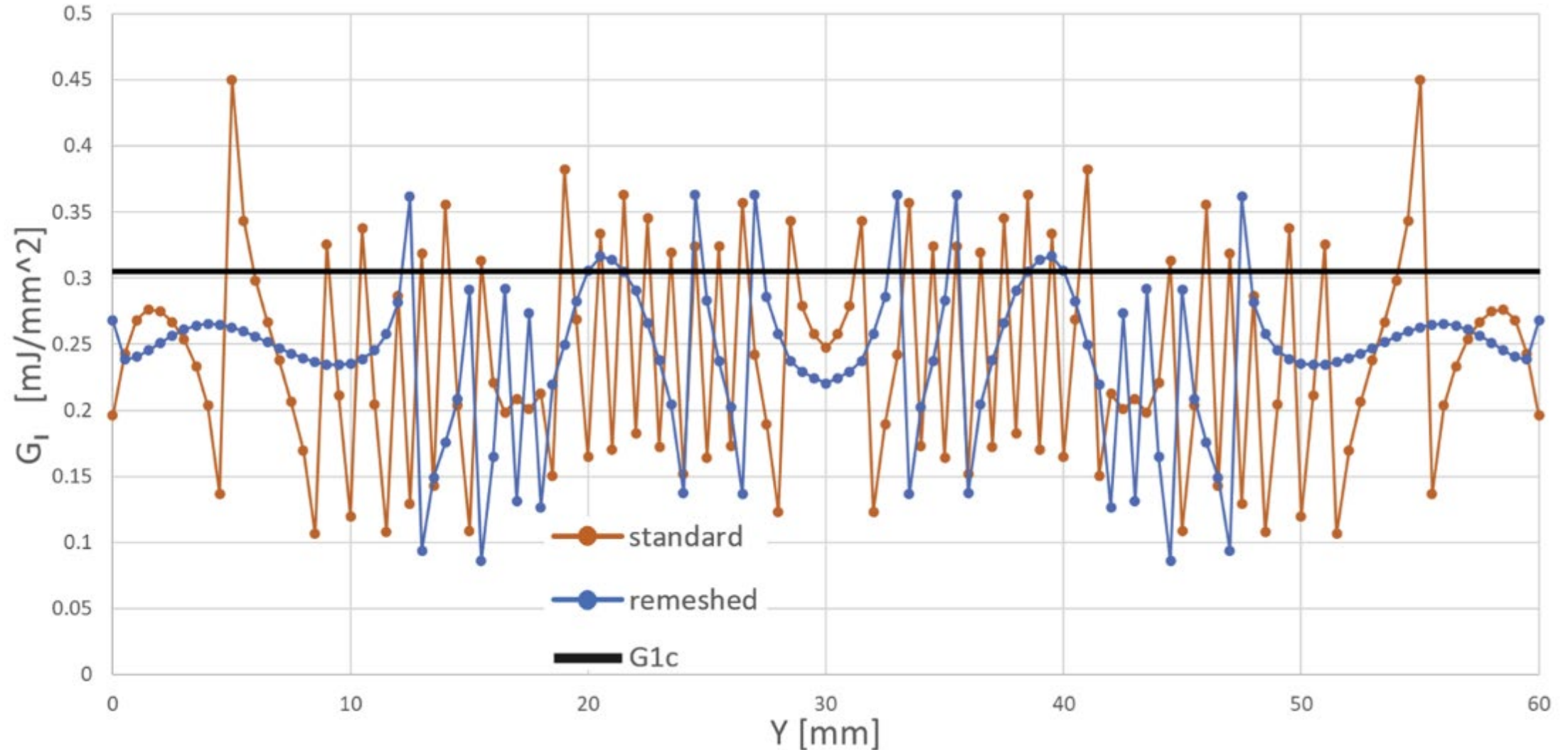
# BOTH TECHNIQUES UNDERESTIMATE THE DELAMINATION RESISTANCE





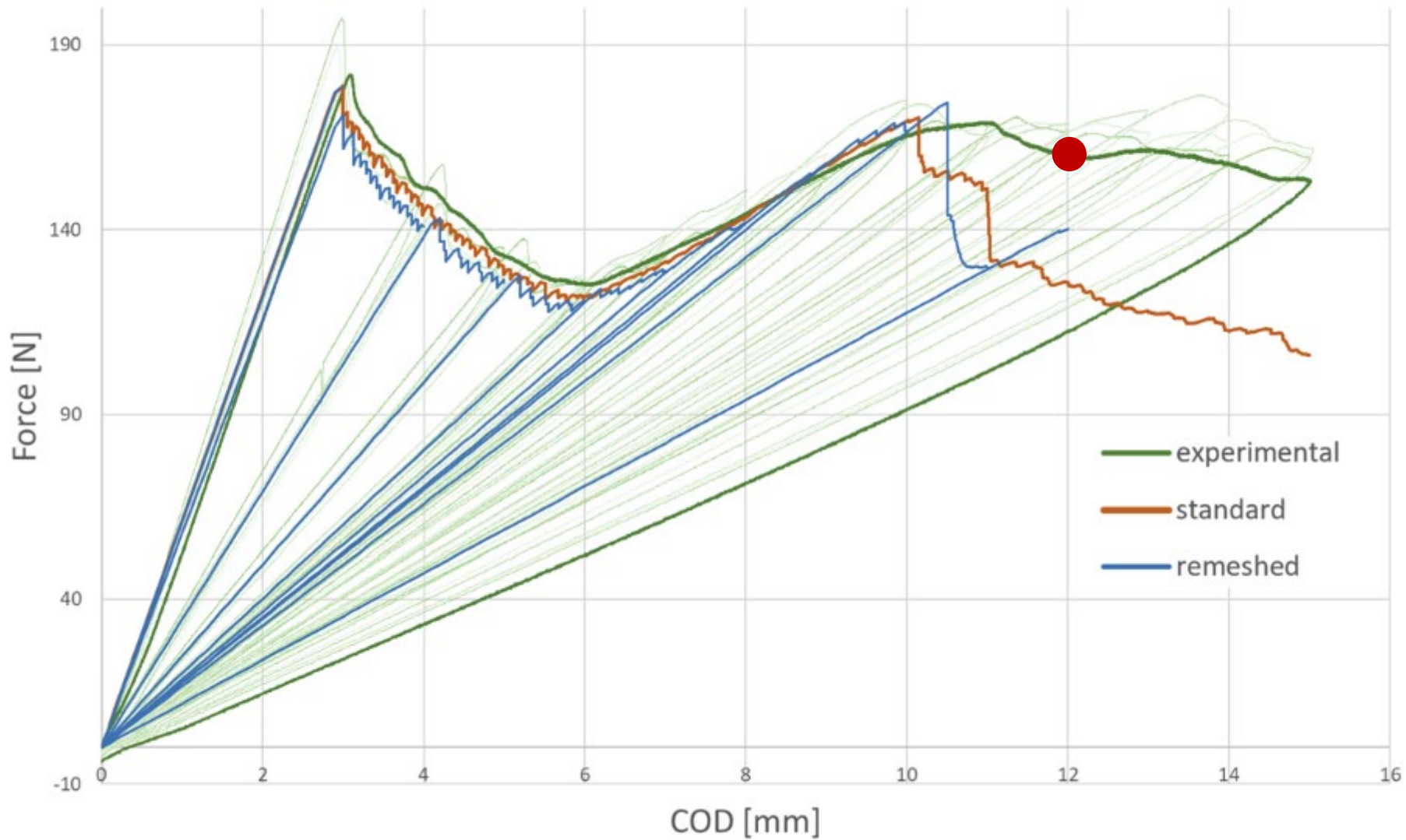
# THE NEW MESH CANNOT COPE WITH SERR CONCENTRATIONS

@ 10 mm propagation





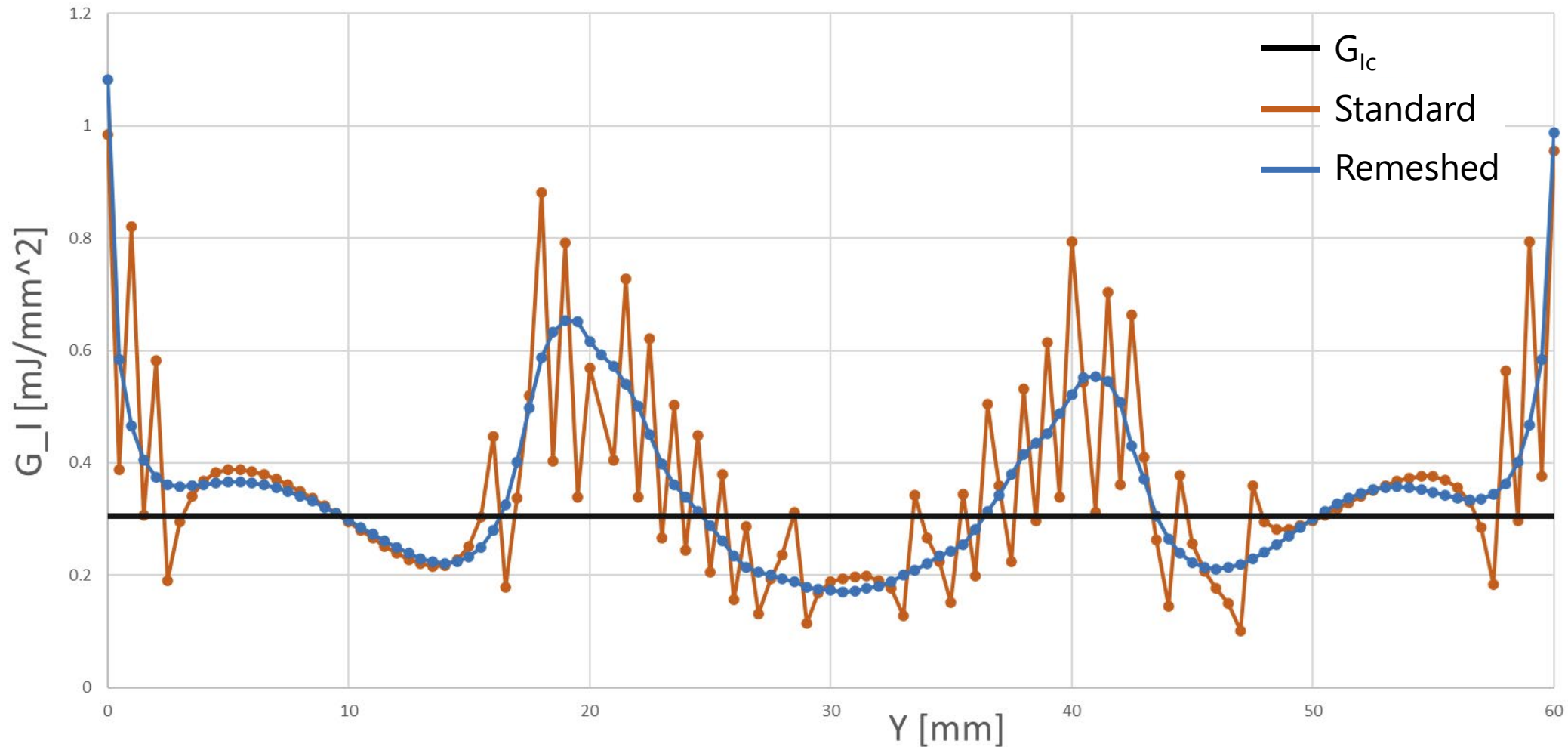
# SIMULATION OF 12 MM DELAMINATION FRONT



# SIMULATION OF 12 MM DELAMINATION FRONT



# SIMULATION OF 12 MM DELAMINATION FRONT

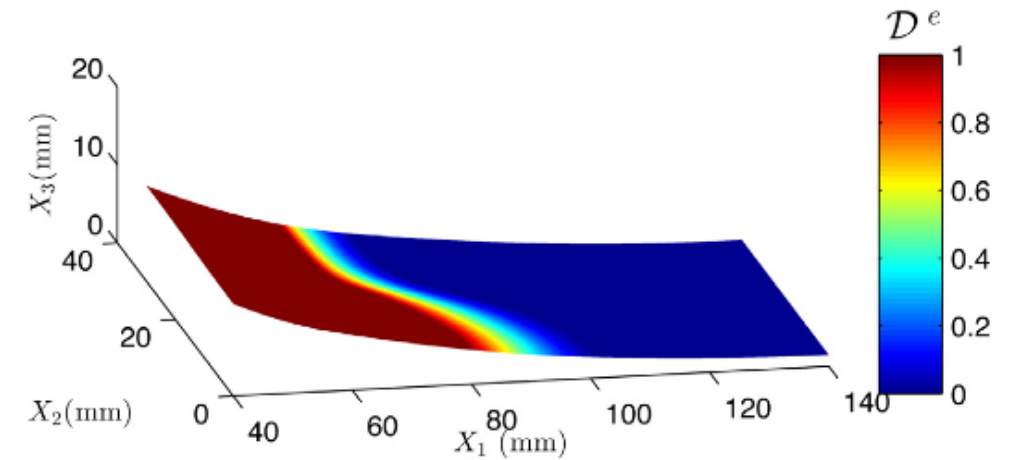


The experimental crack should not be possible **according to VCCT**

# THE EXPERIMENTAL CRACK SHOULD NOT BE POSSIBLE ACCORDING TO VCCT

Possible explanations:

- VCCT is a node-wise technique that does not include a fracture process zone

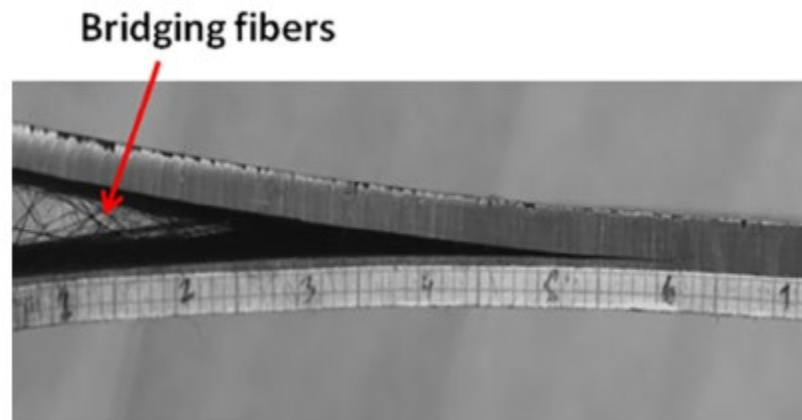


Carreras et al. (2019)

# THE EXPERIMENTAL CRACK SHOULD NOT BE POSSIBLE ACCORDING TO VCCT

Possible explanations:

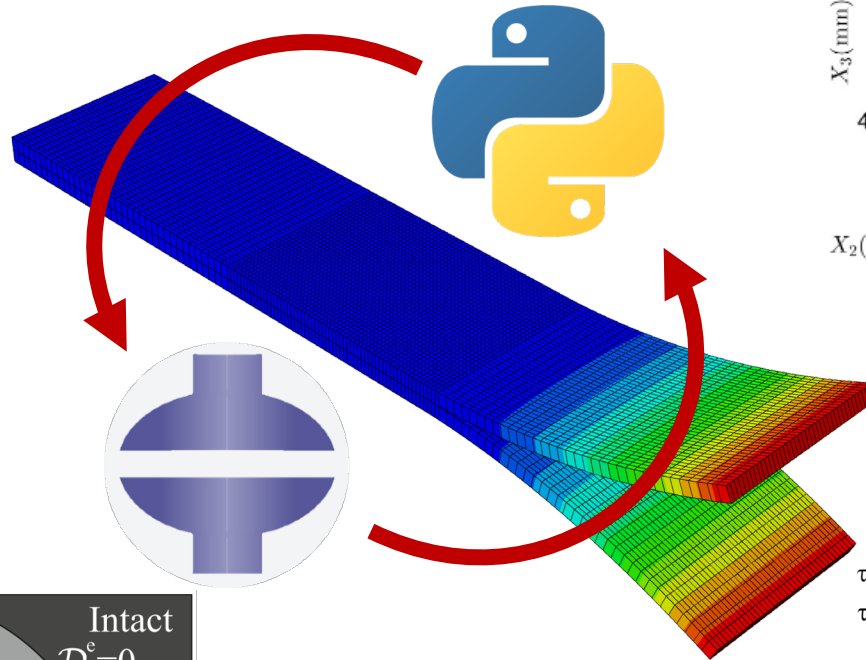
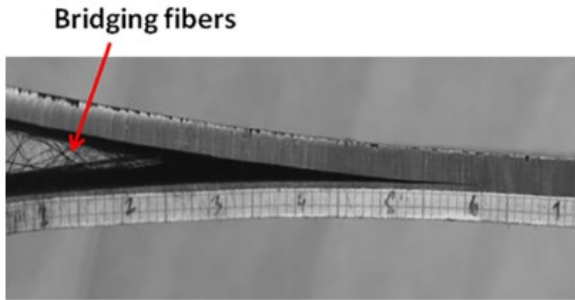
- VCCT is a node-wise technique that does not include a fracture process zone
- Fibre bridging increases local fracture toughness



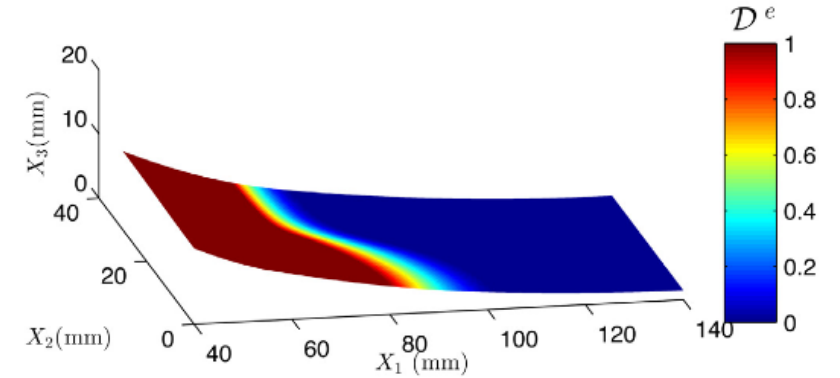
Khan (2019)

# CONCLUSIONS: WHY AM I HERE?

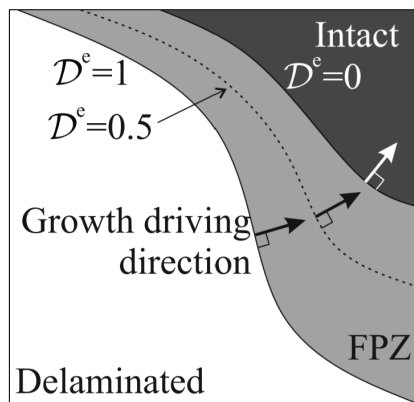
Evolving fracture toughness to model fibre bridging



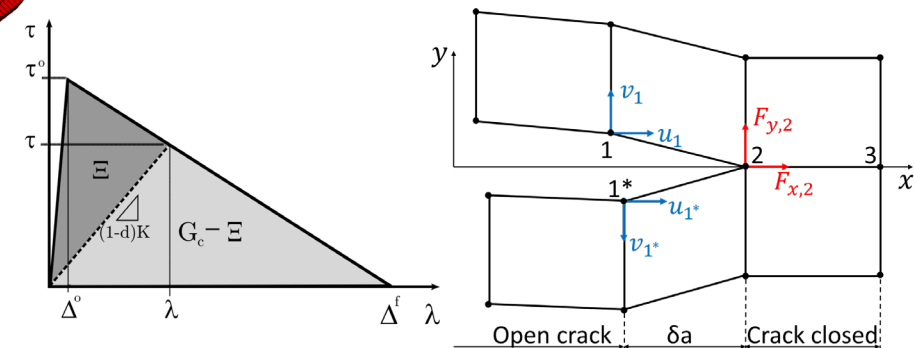
Fracture process zone in VCCT



Evaluate modes decomposition with remeshed VCCT



Hybrid CZM-VCCT







## CONTACTS



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